

DOT/FAA/EE/93-03 DOT-VNTSC-FAA-93-19

Office of Environment and Energy Washington, DC 20591 INM

Integrated Noise Model Version 4.11

User's Guide - Supplement

Gregg G. Flerning John R. D'Aprile

John A. Volpe National Transportation Systems Center Acoustics Facility Cambridge, MA 02142-1093 S DTIC
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Final Report December 1993

Supplement to Report No. DOT/FAA/EE/92/02

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# REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collectime for reviewing instructions, search completing and reviewing the collection aspect of this collection of information Services, Directorate for information Of 2202-4302, and to the Office of Manager	tion of information is estimated to average ing existing data sources, gathering and m of information. Send comments regarding of including suggestions for reducing this perations and Reports, 1215 Jefferson Davi ment and Budget. Paperwork Reduction Proje	e 1 hour per response, including the mintaining the data needed, and this burden estimate or any other burden, to Washington Headquarters & Highway, Suite 1204, Arlington, VA ct (0704-0188), Mashington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)	3. REPORT TYPE AND DATES COVERED Final Report June 1992 - December 1993					
4. TITLE AND SUBTITLE INM, Integrated Noise Model V User's Guide - Supplement	5. FUNDING NUMBERS FA465/A4012					
6. AUTHOR(S) Gregg G. Fleming, Edward J. I John R. D'Aprile						
7. PERFORMING ORGANIZATION NAME(S) AND A U.S. Department of Transporta Research and Special Programs Volpe National Transportation Cambridge, MA 02142	8. PERFORMING ORGANIZATION REPORT NUMBER  DOT-VNTSC-FAA-93-19					
9. SPONSORING/MONITORING AGENCY NAME(S) U.S. Department of Transports Federal Aviation Administration of Environment and Enc. 800 Independence Avenue, S.W Washington, DC 20591	10. SPONSORING/MONITORING AGENCY REPORT NUMBER DOT/FAA/EE/93-03					
11. SUPPLEMENTARY NOTES  1 Technology & Management Systems, Inc. 99 South Bedford Street, Suite 211 Burlington, MA 01803-5128	. <sup>2</sup> Unisys Corporation Kendall Square Cambridge, NA 02142					
	the public through the Natio	nal 12b. DISTRIBUTION CODE				
Technical Information Service, Springfield, VA 22161  13. ABSTRACT (Maximum 200 words)  The John A. Volpe National Transportation Systems Center (Volpe Center), in support of the Federal Aviation administration, Office of Environment and Energy, has developed Version 4.11 of the Integrated Noise Model (INM). The User's Guide for the Version 4.11 computer software is a supplement to INM, Version 3, User's Guide - Revision 1 for the Version 3.10 computer software released in June, 1992. The Version 4.11 supplement, prepared by the Volpe Center's Acoustics Facility, presents computer system requirements as well as installation procedures and enhancements. Specific enhancements discussed include: (1) the introduction of a takeoff profile generator; (2) the ability to account for terrain elevation around a specified airport; (3) the ability to compute the CNEL, WECPNL, LEQDAY, and LEQNIGHT noise metrics; (4) the						

•	er Model, Noise Contou	_	15. NUMBER OF PAGES 82
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17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT

ability to account for airplane runup operations; (5) the ability to account for displaced runway thresholds during approach operations; (6) an enhancement to the noise contour computations: (7) an increase in the number of takeoff profile segments;

and (8) enhancements to the echo file.

## PREFACE

This document was prepared by the John A. Volpe National Transportation Systems Center (Volpe Center), in support of the Federal Aviation Administration, Office of Environment and Energy. It is a User's Guide for the Integrated Noise Model (INM) Version 4.11 computer software used to predict noise impact around airports. This User's Guide is a supplement to INM, Version 3, User's Guide - Revision 1, which was released in June, 1992, along with the INM Version 3.10 computer software. The Version 4.11 supplement, prepared by the Volpe Center's Acoustics Facility, presents computer system requirements as well as installation procedures and INM Version 4.11 enhancements.

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## 1. INTRODUCTION

During June, 1992, through December, 1993, the John A. Volpe National Transportation Systems Center (Volpe Center), in support of the Federal Aviation Administration, Office of Environment and Energy, developed Version 4.11 of the Integrated Noise Model (INM). The User's Guide for the Version 4.11 computer software, prepared by the Volpe Center's Acoustics Facility, is a supplement to the Integrated Noise Model (INM), Version 3, User's Guide - Revision 11 for the Version 3.10 computer software released in June, 1992. Section 1.0 of the supplementary document presents computer system requirements and installation procedures for INM Version 4.11. Section 2.0 describes the user's implementation of several new capabilities, including descriptive examples. Appendix A describes the technical revisions made to several internal algorithms primarily revisions which are transparent to INM users. Appendices B and C, respectively, present a technical discussion of two new capabilities, the takeoff profile generator and the capability to account for airplane runup operations. Appendix D presents a copy of the INM Input Testcase, revised to reflect INM Version 4.11 enhancements. Appendix E contains a copy of the User's Manual for the WINM computer software, an INM Version 4.11 plotting program for use with Microsoft Windows.

## 1.1 Computer System Requirements

INM Version 4.11 operates on an IBM Personal Computer (PC)-Compatible platform with the following minimum configuration:

- IBM PC-AT or compatible, Series 286 microprocessor;
- 3 MB of available hard disk space;
- 590 KB of Random Access Memory (RAM) or 3 MB of RAM, if operating the INM from a RAM disk, as discussed in Section 1.2.1 below;
- Math co-processor, Series 80287; and
- Microsoft-compatible Disk Operating System (MSDOS) Version 3.3.

In addition, the CONFIG.SYS file on the PC slated for INM Version 4.11 installation must contain the following lines: BUFFERS=30; and FILES=30.

### 1.2 Installation

The files on the INM Version 4.11 system diskette have been stored in a compressed format using the PKZIP Version 1.1 utility software [Copyright (c) 1990 PKWare, Inc.]. With the source drive prompt displayed on the screen, execute the UNPACK batch file to install INM Version 4.11 on your PC:

## • UNPACK <SOURCE DRIVE> <TARGET DRIVE>

For example, the command UNPACK A C will install, from the A drive, INM Version 4.11 on the C drive in a subdirectory called INM411. Note: The UNPACK batch file will, without prompting, overwrite the contents of subdirectory INM411, if one exists on the user-specified target drive.

#### 1.2.1 RAM Disk Installation

Operation of INM Version 4.11 on a RAM disk will improve computation time by an estimated 5 to 15 percent, as compared to operating it from a hard-disk drive. RAMDRIVE.SYS, an installable device driver supplied with Microsoft-compatible DOS, allows a user to configure part of the PC's RAM as if it were a hard disk (i.e., a RAM disk, sometimes referred to as a virtual disk). The following is an example installation of INM Version 4.11 onto a RAM disk. The user is referred to the DOS manual and/or the manual supplied with any memory management software being used if difficulties should occur.

To install RAMDRIVE.SYS for use with INM Version 4.11, the following command line should be included in the CONFIG.SYS file:

#### DEVICE=C:\DOS\RANDRIVE.SYS 3000/E

Upon including the above command line in the CONFIG.SYS file, the PC must be rebooted. After rebooting, the PC will have a 3 MB RAM drive located in extended memory. The RAM drive's logical, alphabetical drive designation will be one letter higher than the highest current physical drive on the PC (e.g., if a PC has a 5% inch Adrive, a 3% inch B-drive, and a hard-disk C-drive, upon rebooting, the RAM drive will be designated the D-drive). The user may now install the INM software on the RAM drive by designating it as the target drive for installation. For example:

## A:\UNPACK A D

The above command will automatically install the INM from the A-drive onto a subdirectory (INM411) on the RAM drive (i.e., in this example the D-drive). The RAM drive must now be logically connected to the hard drive using DOS's JOIN command. To accomplish this, an empty subdirectory, e.g., C:\RAM, must be created on the hard drive. From within that subdirectory execute the following command:

## C:\RAM\JOIN D: C:

This will assign the RAM drive, i.e., the D-drive, to operate within the subdirectory C:\RAM on the hard drive. Note: It is extremely important to remember that each time the PC is reset or its power is turned off, the information stored on the RAM drive will be lost. As a result, i. the INM is run from the RAM drive, all files must be copied to a physical drive, e.g., a floppy drive, prior to powering-off the PC.

## 2. IMPLEMENTATION OF INM VERSION 4.11 ENHANCEMENTS

This Section of the document describes the methodology for implementing INM Version 4.11 enhancements. It includes a background discussion of the enhancements, a brief discussion of the need for the enhancements, and example implementation of the enhancements. The following enhancements are discussed: (1) the takeoff profile generator; (2) the ability to account for terrain elevation around a specified airport; (3) the ability to compute the CNEL, WECPNL, LEQDAY, and LEQNIGHT noise metrics; (4) the ability to account for airplane runup operations; (5) the ability to account for runway thresholds during approach operations; (6) an enhancement to the noise contour computations; (7) an increase in the number of takeoff profile segments; and (8) enhancements to the echo file.

#### 2.1 Takeoff Profile Generator

This enhancement allows for the computation of airplane takeoff profiles based on the user-supplied airport elevation and temperature entry in the SETUP section of the INM input file. The takeoff profiles are utilized by the INM in the computation of all noise metrics. Previous versions of the INM utilize takeoff profiles which were based on standard-day conditions, i.e., temperature of 59°F and airport elevation of zero ft Above Mean Sea Level (MSL). Previously, the user-supplied airport elevation (altitude) and temperature were only used to compute an atmospheric acoustic impedance correction.

The takeoff profile generator is made possible by the inclusion of standardized airplane operating procedures and performance coefficients in Data Base Number 11. procedures and coefficients are presented in References 2, 3, and 4, and accessible from the Data Base using the ACDB11.EXE computer program, supplied with the Version 4.11 release. With the exception of INM airplane numbers 1, 6, 7, 8, 10, 24, 56, 100, 101, and four of the new airplanes (INM airplane numbers 104 to 107) discussed further in Appendix A, the operating procedures and performance coefficients required for takeoff profile computation are included in Data Base Number For the airplanes without standard procedures and coefficients the takeoff profile for standard conditions is assumed regardless of the airport elevation and temperature. Note: The incorporation of the takeoff profile generator will not affect the standard approach profiles. The approach profiles are the same as employed in INM Version 3.10.

Operation of the profile generator is time-efficient and entirely transparent to the user. If other than standard-day conditions are specified by the user in the SETUP portion of the input file, the profile generator automatically computes the takeoff profiles using the airplane performance coefficients in Data Base Number 11 and the equations in the

Society of Automotive Engineers Aerospace Information Report 1845<sup>5</sup> (SAE/AIR 1845). When an airport elevation and temperature is not specified, the INM assumes standard conditions and utilizes the standard profiles included with Data Base Number 11, i.e., the internal profile generator will not be exercised.

To insure the takeoff profiles and resultant noise metrics computed by INM Version 4.11 are reasonable for the user-defined input case, a runway length check has been instituted. When the computed ground roll segment of the takeoff profile exceeds the user-specified runway length, the user is notified of the discrepancy. A message similar to the following is included in the echo file.

 WARNING: COMPUTED GROUND ROLL ERROR FOR INM AIRPLANE 747200, STAGE WEIGHT 7, -- EXCEEDS USER-DEFINED RUNWAY LENGTH BY X PERCENT FOR THE TAKEOFF ON TRACK TR1, RUNWAY 091.

In main, cases this warning will indicate to the user that there is an error in the input file, possibly in the user-defined average yearly temperature, airport elevation, airport runway length, or airplane stage weight. In cases where the computed ground roll segment exceeds the runway length by more than 10 percent, the above message will be included in the echo file as a fatal error rather than a warning and the user will not be permitted to continue processing of the input case.

There may be instances where the user has correctly defined the input case and the computed ground roll segment exceeds the runway length by more than 10 percent. This apparent anomaly may be the result of using the average yearly temperature at the airport as an input. For example, a particular airport may be capable of operating a high stageweight B747 airplane in the early evening or during winter months only, when the temperature is significantly lower than the average yearly temperature. In such cases it is suggested that a user-defined profile be included in the input file.

In addition, there may be instances (e.g., high stage weights, high temperatures, and high airport elevations combined) where a negative rate-of-climb is computed. Consequently, a fatal error will occur and a profile will not be generated. In such instances, the user will be notified with a message similar to that below; it is suggested that a user-defined profile be included in the input file.

• FATAL: PROFILE FOR INM AIRPLANE 747200, STAGE WEIGHT 7 CANNOT BE COMPUTED.

A technical discussion of the takeoff profile generator is presented in Appendix B. In addition, Appendix B presents tables which summarize the runway requirements and operational boundaries of the profile generator. These tables are presented for various combinations of airport elevation and temperature intended to cover the range of average yearly conditions at airports across the United States.

#### 2.2 Terrain Elevation

This user-selectable enhancement included with INM Version 4.11 allows for the computation of source-to-receiver slant range, i.e., propagation distance, based upon actual terrain elevation at receiver locations around a specified airport. The implementation of this enhancement can result in a vast improvement in the accuracy of the noise computations at located hilly terrain, airports near however implementation will result in an increase in computation time by an estimated 50 to 100 percent. To utilize this enhancement, INM Version 4.11 users must have the United States Geological Survey (USGS) 3 Arc Second Elevation Data on CD-ROM, available from:

Rocky Mountain Communications, Inc. (RMC) 2023 Montane Drive East Golden, CO 80401 (303) 526-5454 (303) 526-2662 (FAX)

The USGS data are available for the entire United States or parts thereof.

Prior to implementing the elevation enhancement within INM Version 4.11, the preprocessing program, MAKEFILE.EXE, which is included with the Version 4.11 distribution package, must be run on the RMC Digital Elevation Model (DEM) files. MAKEFILE.EXE constructs a 2.8 MB, one-degree by one-degree, geodetic data file with the user-specified airport located at the geographic center of the file. The file generated by MAKEFILE.EXE, which has a three-letter user-defined prefix and a .3CD extension (e.g., Boston's Logan International Airport might be designated BOS.3CD), will be used by INM Version 4.11 to compute the source-to-receiver slant range. Use of the MAKEFILE.EXE program is described below.

With the drive prompt displayed on the screen, type MAKEFILE to invoke the program.

## • C:\INM411\ MAKEFILE

MAKEFILE.EXE will then prompt the user to enter a three-letter airport identification, e.g., BOS, and the latitude and

longitude of a reference point at the airport (e.g., the beginning of the primary runway). In the following example the latitude and longitude are for the start of Runway 09L at Boston-Logan.

- e ENTER 3 LETTER AIRPORT IDENTIFIER (EX. BOS): BOS
- e ENTER RUNWAY LAT COORD. DEGS MINS SECS (EX. 42 21 20): 42 21 20
- ENTER RUNWAY LON COORD. DEGS MINS SECS (EX. 71 00 48): 71 00 48

The MAKEFILE.EXE program then computes the coordinates of the southeast corner of a one-degree by one-degree data-block based upon the start of the airport's primary runway being at the geographic center of the block. The computed southeast corner is displayed along with the four RMC DEM files required to construct the one-degree Ly one-degree data-block around the airport. The user is also given the option to overwrite an existing or create a new BOS.3CD file, where BOS is the three-letter airport identifier.

- THE SE CORNER OF THE REQUIRED (1X1 DEG) DATA BLOCK IS: 41 52 70 31
- THE REQUIRED DEM FILES ARE: NW FN=42071.3CD NE FN=42070.3CD SW FN=41071.3CD SE FN=41070.3CD
- DO YOU WISH TO CREATE A NEW BOS.3CD FILE (Y/N) ? Y

The user should type  $\underline{Y}$  to overwrite/create a new file. If the four DEM files exist in the current directory, the program will create the BOS.3CD file without further prompting. MAKEFILE.EXE cannot find the required DEM files, it will request that the user enter the drive where the DEM files are resident. In addition, MAKEFILE.EXE will ask if the data are on the RMC CD-ROM and, if so, copy them into the current directory. If the four DEM files are not on the CD-ROM drive, MAKEFILE.EXE will request the path where the files can be The program will then construct the required onefound. degree by one-degree data-file, with the airport's primary runway at its approximate geographic center. The user will be informed that the file has been constructed, and the minimum and maximum elevation within the constructed one-degree by one-degree block will be provided.

#### WRITING OF BOS.3CD IS COMPLETE

The example BOS.3CD file is now ready for implementation by the INM. To utilize the elevation data in the BOS.3CD file in the computation of source-to-receiver slant range, the user must specify, in the SETUP portion of the INM input file: (1) the three-letter airport code which identifies the specific user pre-processed .3CD file; (2) the disk-drive location of the .3CD file (Note: It is not necessary to specify the location of the .3CD file if it is in the current directory; also, if the .3CD file resides in a subdirectory, the path to that subdirectory must be created prior to running INM.); and (3) the latitude and longitude of a user-defined reference point at the airport, where the X and Y coordinates of all defined runways must be referenced to this point. To insure that the user has identified the appropriate .3CD file, the INPUT.EXE program will test the user-defined reference point at the airport against the stored reference in the .3CD file.

In the following example the user has: (1) specified Boston's Logan International Airport; (2) identified the C-drive as the location for the BOS.3CD file; and (3) specified the latitude and longitude of a reference point at Boston-Logan.

#### • SETUP:

TITLE <EXAMPLE IMPLEMENTATION OF ELEVATION ENHANCEMENT>
AIRPORT <ELEVATION EXAMPLE>

CODE BOS
DRIVE C
LATITUDE 42 21 20
LONGITUDE 71 00 48

With the elevation enhancement invoked as described above, all noise-level computations are performed based upon the actual source-to-receiver slant range, rather than assuming a flat terrain as was the case in previous versions of the INM.

In addition, the data in the BOS.3CD file are used to compute the slope of a three-by-three arc-second tangential ground plane, with the receiver at its physical center. This ground plane is used in the computation of the source-to-receiver elevation-angle, beta, required by the lateral attenuation algorithm in the INM. The beta angle is defined as the angle subtended by the propagation path from the airplane to the receiver and the three-by-three arc-second ground plane. Figures 2-1 and 2-2, respectively, depict the beta angle for two scenarios: (1) previous versions of the INM (i.e., flat terrain); and (2) INM Version 4.11.

## 2.3 CNEL, WECPNL, LEQDAY, and LEQNIGHT Noise Metrics

The capability to compute four additional noise metrics has been included in INM Version 4.11. They are the Community Noise Equivalent Level (CNEL), Weighted Equivalent Continuous Perceived Noise Level (WECPNL), Equivalent Sound Level During Daytime Hours (LEQDAY), and Equivalent Sound Level During Nighttime Hours (LEQNIGHT). The addition of these four metrics brings the total number of metrics available for computation by the INM to eight (NEF, LEQ, LDN, TA, CNEL, WECPNL, LEQDAY, and LEQNIGHT). As was the case in previous

# Scenario 1

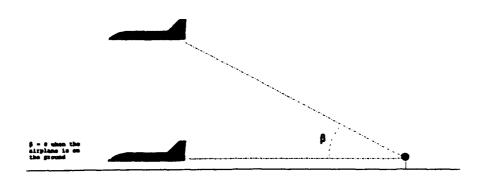


FIGURE 2-1: BETA ANGLE FOR INM VERSION 3.10 AND BEFORE

# Scenario 2

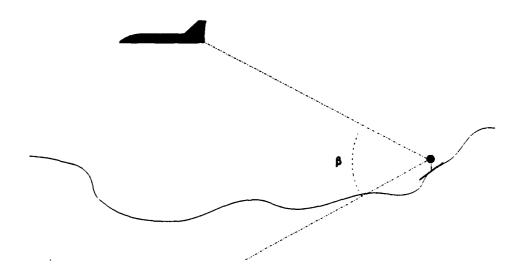


FIGURE 2-2: BETA ANGLE FOR INM VERSION 4.11

versions of the INM, Version 4.11 allows for the computation of all metrics simultaneously in grid mode or a single user-defined metric in contour mode for a given input case. A brief description of the CNEL, WECPNL, LEQDAY, and LEQNIGHT noise metrics follows:

(1) Community Noise Equivalent Level (CNEL): The CNEL noise metric, which is primarily used in California, is similar to the Day-Night Sound Level (LDN) metric in that it incorporates the energy-averaged A-weighted sound level integrated over a 24-hour period. However, unlike LDN, CNEL incorporates an additional penalty for operations occurring between the evening hours of 1900 and 2200 hours. For CNEL, a 3 dB penalty is applied to operations occurring between 1900 and 2200 hours, and a 10 dB penalty is applied to operations occurring between 2200 and 0700 hours. The equation for computing CNEL within the INM is as follows:

CNEL = SEL +  $10\log_{10}(N_{day} + 3N_{eve} + 10N_{night}) - 49.4$ ,

where SEL = Sound Exposure Level in dBA;

 $N_{day}$  = number of operations between 0700 and 1900 hours local time;

N<sub>eve</sub> = number of operations between 1900 and 2200 hours local time;

 $N_{\text{night}}$  = number of operations between 2200 and 0700 hours local time;

and 49.4 = constant which normalizes CNEL to a 24-hour period, (i.e., 10log<sub>10</sub> (1/86,400 sec/day) = -49.4).

(2) Weighted Equivalent Continuous Perceived Noise Level (WECPNL): The WECPNL noise metric, which is primarily used by the European Community, is based upon the PNLT noise metric and is computed within the INM as follows:

WECPNL = EPNL +  $10\log_{10}(N_{day} + 3N_{eve} + 10N_{night}) - 39.4$ ,

where all definitions are the same as in CNEL, above, except:

EPNL = Effective Perceived Noise Level in dB; and

39.4 = (49.4 - 10); where 49.4 is the constant which normalizes WECPNL to a 24-hour period,

(i.e.,  $10\log_{10}(1/86,400 \text{ secs/day}) = -49.4$ ); and -10 is the duration normalizing factor in the definition of EPNL.<sup>6</sup>

(3) Equivalent Sound Level During Daytime Hours (LEODAY): The LEQDAY noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (dBA) normalized to the 15-hour time period from 0700 to 2200. The equation for computing LEQDAY within the INM is as follows:

LEQDAY = SEL +  $10\log_{10}(N_{day} + N_{eve}) - 47.3$ ,

where all definitions are the same as in CNEL, above, except:

- 47.3 = constant which normalizes LEQDAY to the 15-hour period from 0700 to 2200, (i.e.,  $10\log_{10}(1/54,000 \text{ sec}) = -47.3$ ).
- (4) Equivalent Sound Level During Nighttime Hours (LEONIGHT): The LEQNIGHT noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (dBA) normalized to the 9-hour time period from 2200 to 0700. The equation for computing LEQNIGHT within the INM is as follows:

LEQNIGHT = SEL +  $10log_{10}(N_{night})$  - 45.1,

where all definitions are the same as in CNEL, above, except:

45.1 = constant which normalizes LEQNIGHT to the 9-hour period from 2200 to 0700, (i.e.,  $10\log_{10}(1/32,400 \text{ sec}) = -45.1$ ).

## 2.4 Airplane Runup Operations

This enhancement allows INM Version 4.11 to compute noise levels due to airplane engine runup operations. The need for this particular enhancement is recognized primarily around airplane maintenance facilities. To invoke this capability the user must define an airplane runup in the TAKEOFF section of the input file as follows:

• INT.NM.
TAKEOFFS BY FREQUENCY:

TRACK RU1 RWY 09L STRAIGHT 50

OPERATION 747200 RUNUP 1 D=30

OPERATION 747200 STAGE 4 D=80

<OR>
OPERATION 747200 STAGE 4 D=80 RUNUP 1 D=30

In the above example, a 30 second (D=30) runup operation is defined for a B747-200 airplane operation at the thrust setting of Stage Weight 1. The runup, as specified, takes place on a runway designated as 09L and a track designated as RU1. STRAIGHT 50 defines the length of the track in nautical miles. In fact, the track length for runup operations is ignored in the computation of runup noise. For runup noise computations it is assumed that the airplane covers a track with an arbitrarily chosen fixed length of 20 ft. The specific location and heading of the runup operation in the above example must be defined in the RUNWAYS section of the input file as shown in the following:

## RUNWAYS

RW 09L-27R 0 0 TO 9487 -497

In the above example, the runup operation takes place at the start of an active runway, i.e., Runway 09L. If the user wants to define a runup operation at a location at the airport other than on an active runway, e.g., at a maintenance facility, then the maintenance facility must be defined as if it were a runway. Here it is suggested that a maintenance facility, or any other location specified for a runup operation, be defined as a runway which is 20 ft in length. The definition of a maintenance facility as a 20 ft runway is shown in the following example.

#### RUNWAYS

RW 13-31 0 5000 TO 20 5000

The above runup definitions assume that the full-power takeoff thrust associated with the user-defined stage weight is maintained for the duration of the runup. However, runup operations can occur at other than full-power thrust. To model such instances, a user-defined runup should be included in the input file as follows:

# AIRCRAFT:

TYPES

AC 747200 STAGE 1=RU

## PROFILES TAKEOFF

PF RU SEGMENTS=3 WEIGHT=525000 ENGINES=4

 DISTANCES
 0
 10
 20

 ALTITUDES
 0
 0
 0

 SPEEDS
 160
 160
 160

 THRUSTS
 35022
 35022

INT.NM.

TAKEOFFS BY FREQUENCY:

TRACK RU1 RWY 09L STRAIGHT 50
OPERATION 747200 RUNUP 1 D=30

In addition, the specific location, e.g., the start of a runway or at a maintenance facility, and heading of the runup operation in the above user-defined example must be specified in the RUNWAYS section of the input file as discussed earlier in this section. A technical discussion of the airplane engine runup capability is presented in Appendix C.

# 2.5 Approach Runway Thresholds

The capability to account for displaced runway thresholds for approach operations has been added to INM Version 4.11. previous versions of the INM, the runway touch-down point was assumed to be a fixed 954 ft from the edge of the runway for airplanes with a three degree approach glide slope, and 572 ft for the four airplanes with a five degree approach glide slope (INM airplane numbers 74 to 77). With INM Version 4.11, a user-defined displaced threshold (DT), either positive or negative, is added to the fixed runway touch-down point. insure realistic DT's are defined by the user, they are checked versus the runway coordinates. If discrepancies exist, the user is notified in the echo file, as appropriate. In the following example, a 1454 ft runway touch-down point has been defined in the SETUP section of the input file for Runway 09L (i.e., 500 ft for the user-defined DT plus 954 ft for the fixed touch-down point); and a runway touch-down point of 954 ft has been defined for Runway 27R:

## • SETUP:

TITLE <EXAMPLE IMPLEMENTATION OF APPROACH RUNWAY THRESHOLD>
AIRPORT <RUNWAY THRESHOLD EXAMPLE>

ALTITUDE 23
TEMPERATURE 12.66 C

#### RUNWAYS

RW 09L-27R 0 0 <u>DT 500</u> TO 9487 -497 <u>DT 0</u> <OR>
RW 09L-27R 0 0 <u>DT 500</u> TO 9487 -497

The above runway definition is depicted graphically below:

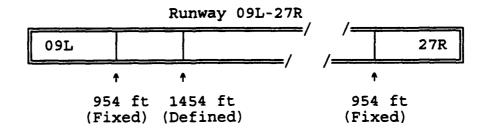


FIGURE 2-3: RUNWAY DEFINITION

The inclusion of the 500 ft user-defined DT results in a runway touchdown point 1454 ft from the start of Runway 09L (i.e., 500 ft for the user-defined DT plus 954 ft for the fixed touch-down point).

# 2.6 Noise Contour Computations

INM Version 4.11 provides, in the echo file, a warning to users when there are insufficient grid points to accurately compute a specific noise contour. In previous versions, the INM would automatically make the determination that there were insufficient grid points, and return a run-time error to the computer display without further explanation. The INM's noise computation window must be redefined to encompass additional grid points in the area of interest.

If the user-defined computational window is too coarse to allow computation of a requested contour or the requested contour is not encompassed by the window, INM Version 4.11 will include a message in the echo file which is similar to the following:

• CONTOUR CONTOUR AREA LEVEL (SQ. MILES)

CN 3 \*WARNING: LDN 30.0 CONTOUR DOES NOT EXIST

In the above example, the defined window was either too coarse to reliably compute the user-requested 30 dB LDN contour or the contour was not encompassed by the window.

## 2.7 Takeoff Profile Segments

INM Version 4.11 provides for user-defined takeoff profiles with up to 18 segments. Previous versions of the INM limited the number of segments to 14. This enhancement allows for more precise user-defined takeoff profiles. It will also more easily facilitate the incorporation of a flight-procedure generator planned for a future version of the INM, since certain procedures may require higher resolution profiles, and thus more segments.

## 2.8 Echo File

All output reports generated by INM Version 4.11 have been modified to account for the enhanced capabilities discussed in Section 2.0, above.

#### 3. REFERENCES

- Flythe, M.C., <u>Integrated Noise Model Version 3. User's Guide Revision 1</u>, Report No. DOT/FAA/EE-92/02, Arlington, VA: CACI, Inc. Federal, June 1992.
- Bishop, D.E., Mills, J.F., <u>Update of Aircraft Profile Data for the Integrated Noise Model Computer Program, Volume 1</u>, Report No. FAA-EE-91-02, Canoga Park, CA: Acoustical Analysis Associates, Inc., March 1992.
- Bishop, D.E., Mills, J.F., <u>Update of Aircraft Profile Data for the Integrated Noise Model Computer Program, Volume 2</u>, Report No. FAA-EE-91-02, Canoga Park, CA: Acoustical Analysis Associates, Inc., March 1992.
- Bishop, D.E., Mills, J.F., <u>Update of Aircraft Profile Data for the Integrated Noise Model Computer Program, Volume 3</u>, Report No. FAA-EE-91-02, Canoga Park, CA: Acoustical Analysis Associates, Inc., March 1992.
- Procedure for the Calculation of Airplane Noise in the Vicinity of Airports, SAE/AIR 1845, Warrendale, PA: Society of Automotive Engineers Committee A-21, Aircraft Noise, 1986.
- Federal Aviation Regulations, Part 36, Noise Standards:
  Aircraft Type and Airworthiness Certification, Washington,
  D.C.: Federal Aviation Administration, December 1988.

#### APPENDIX A

#### REVISIONS TO INM ALGORITHMS

This Appendix discusses, in general terms, revisions to several algorithms and subroutines included in INM Version 4.11. It also discusses the rationale for these revisions and presents their effects on the noise contours, where applicable. The associated computer source code is not included. All revisions discussed below are transparent to the user in that they do not affect useroperation of the INM. However, these revisions will result in more accurate INM noise predictions and an increase in INM computational efficiency. They include: (1) revisions to significance testing within the INM; (2) implementation of a directivity smoothing equation; (3) revisions to the dipole directivity pattern within the INM; and (4) revisions to the INM Data Base.

## A.1 Flight Significance Testing

The methodology employed for determining flight noise significance during grid computations has been streamlined in INM Version 4.11. Rather than looping through each of the first four refinement levels individually and constructing the noise grid on a level-by-level basis, INM Version 4.11 begins by constructing the 17-by-17 point regular grid previously associated with the fourth refinement level, and setting all parameters associated with the 289 total points, including the noise significance flags for each point.

In restructuring the flight significance methodology, it was discovered that INM Version 3.10 was performing unnecessary (i.e., insignificant) noise computations due to improper setting of the flight significance flags. This impropriety had no effect on the computed noise levels but it did increase run-time unnecessarily. Revising the methodology for grid development, including the proper setting of flight significance flags, improved computation time by an estimated 40 percent over INM Version 3.10, for comparable input cases.

## A.2 Directivity Smoothing Equation

The directivity algorithm of SAE/AIR 1845 implemented for receivers behind start-of-takeoff roll, which is based on field-measured data published in 1980, has been maintained within INM Version 4.11. However, a directivity smoothing equation, operating as a function of distance, has been implemented. In previous versions of the INM, the directivity algorithm is applied to noise levels behind start-of-takeoff-roll regardless of lateral distance. In the 1980 study, measurements were made at distances from start-of-takeoff-roll of only 970 to 1280 ft. Recent studies<sup>6,7</sup> have indicated that INM Version 3.10 tends to underpredict noise levels behind start-of-takeoff-roll at distances of 3000 to 5000 ft, well beyond those represented in the 1980 study. This underprediction was especially evident for measurements made directly behind the airplane where

the reduction in noise level due to the directivity algorithm is most pronounced.

As a result, an equation has been incorporated into INM Version 4.11 which smooths out the directivity effect as a function of distance behind the airplane, beginning at a distance of 2500 ft. The smoothing algorithm reduces the directivity effect in decibels by a factor of 50 percent per doubling of distance behind the airplane, beginning at a distance of 2500 ft. For example, a noise level attenuation of 10 dB computed by the directivity algorithm at a distance of 2500 ft will be reduced to 5 dB at 5000 ft due to the smoothing equation.

The smoothing equation built into INM Version 4.11 was empirically and conservatively derived from the data of Reference 6, the more detailed study of the two cited above. However, it is strongly recommended that additional measurments behind start-of-takeoff-roll be performed at a variety of offset distances and azimuth angles at several sites across the country to fine-tune the smoothing equation.

# A.3 Dipole Directivity Pattern

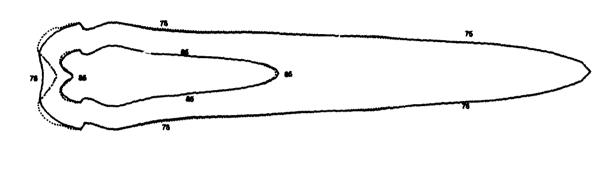
The 90° dipole directivity pattern was originally instituted within the INM as a means of approximating the directivity characteristics Although the exact directivity of an airplane in flight. characteristics are a function of parameters such as airplane type, power setting, speed, and distance, the dipole model has served as a reasonable approximation. In INM Version 4.11, the 90° dipole directivity pattern has been modified. Figures A-1 and A-2 depict the dipole directivity pattern of INM Version 3.10 and earlier modified pattern of INM Version 4.11, and the versions, respectively. For INM Version 4.11, the original dipole directivity directly in front of and behind the airplane has been In addition, the directivity algorithm of SAE/AIR suppressed. 1845, with the addition of the smoothing equation discussed in Section A.2 above, is applied behind the airplane for all modes of operation. See Appendix C for a discussion of the appropriateness of the modified directivity pattern for runup operations.



FIGURE A-1: DIPOLE DIRECTIVITY PATTERN, INM VERSION 3.10 AND BEFORE

FIGURE A-2: MODIFIED DIRECTIVITY PATTERN, INM VERSION 4.11

The effect of the modified directivity pattern on the noise contours is depicted in Figures A-3 and A-4, below. Figure A-3 shows the effect on the SEL footprint for a single takeoff operation of the B737-200 airplane (INM number 47). Figure A-4 shows the effect on the LDN contour for the INM Input Testcase provided with INM Version 3.10.



---- INM VERSION 3.10
AND BEFORE
INM VERSION 4.11

FIGURE A-3: SEL TAKEOFF FOOTPRINT COMPARISON FOR B737-200 AIRPLANE

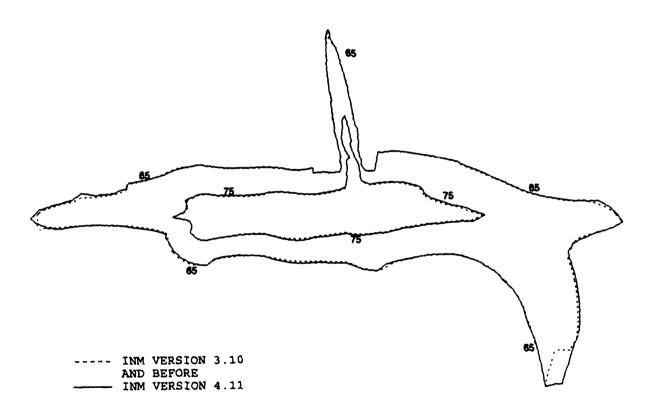


FIGURE A-4: LDN CONTOUR COMPARISON FOR INM INPUT TESTCASE

## A.4 Data Base Number 11

Data Base Number 11 has been created through modifications, consisting primarily of the removal of artifacts from previous versions of the Data Base, and the addition of six new airplanes. As discussed in Section 2.1, Data Base Number 11 was expanded to include airplane performance coefficients and standard flight procedures required for use with the takeoff profile generator. With the exception of INM airplane numbers 1, 6, 7, 8, 10, 24, 56, 100, 101, and four of the new airplanes discussed below, procedures and coefficients required for profile generation are included in the Data Base. For those airplanes without standard flight procedures and coefficients, the takeoff profile for standard conditions is utilized regardless of airport elevation and temperature.

In addition, six new airplanes have been added to Data Base Number 11 (See Table A-1). They include the MD11 with the CF6-80C2D1F and PW4460 engines (INM numbers 102 and 103, respectively), the F-16A with the F100-PW-200 engine (INM number 104), and the F-16C/D with the F110-GE-100, F100-PW-220, and F100-PW-229 engines (INM numbers 105, 106 and 107, respectively). The Noise-Power-Distance (NPD) data, standard-day profiles, performance coefficients and standard flight procedures included in the Data Base for the MD11 airplanes were obtained from the McDonnell Douglas Corporation.

The Volpe Center extracted the NPD data for the F-16 airplanes from the United States Air Force's (USAF) data base which is part of their NOISEMAP suite of computer programs. NOISEMAP, the military counterpart of the INM, is used for predicting noise exposure around airports dominated by military operations. The USAF data were normalized to an airspeed of 160 knots and adjusted for the effect of duration consistent with the procedures for developing the INM data base. The standard-day profiles, which are the same for the four F-16 airplanes, were also extracted from the USAF's data base. They are considered typical for transient F-16 airplanes. However, due to significantly varying takeoff procedures for F-16 airplanes throughout the world a user-defined takeoff profile may be more appropriate.

TABLE A-1: INM VERSION 4.11 DATA BASE AIRPLANE DEFINITION
---

	Airplane Category		Category Noise Apprh				Takeoff Profiles by Trip Length (nm)						
	Name	Description	Name	•	Name	*	0- 500	500- 1000	1000- 1500	1500- 2500	2500- 3500	3500- 4500	over 4500
102	MD11GE	MD-11/CF6-80C2D1F	JCOM	68	2CF68D	102	374	375	376	377	378	379	380
103	MT .1PM	MD-11/PW 4460	JCOM	69	PW4460	103	381	382	383	384	385	386	387
104	P16A	F-16A/PW-200	JMIL	70	PM200	104	388	0	0	0	, ,	0	0
105	F16GE	F-16C/D/GB-100	JMIL	71	GB100	105	369	0	0	0	0	0	0
106	P16PW0	F-16C/D/PW-220	JMIL	72	PW220	106	390	0	0	0	0	0	0
107	P16PW9	P-16C/D/PH-229	JMIL	73	PW229	107	391	0	0	0	0	0	0

## A.5 References

- Horonjeff, R.D., <u>Analysis of Aircraft Noise Levels in the Vicinity of Start-of-Takeoff Roll at Baltimore-Washington International Airport</u>, Report No. FAA-EE-92-01, Lexington, MA: Harris Miller Miller & Hanson Inc., May 1992.
- Brown-Buntin Associates, "Letter Report, Noise Contour Adjustments McCarran International Airport, Las Vegas Unpublished Data", August 1993.

#### APPENDIX B

## TAKEOFF PROFILE GENERATOR

This Appendix presents a technical discussion of the takeoff profile generator within INM Version 4.11. The discussion, based on the algorithms of SAE/AIR 1845 and the aerodynamic coefficients and standard flight procedures in Data Base Number 11, is presented in two sections. The first section describes the computation of individual takeoff profile segments under standard conditions, i.e., airport temperature of 59°F and airport elevation of zero ft Above Mean Sea Level (MSL). The second section describes the computation of individual takeoff profile segments under non-standard conditions.

The horizontal distance and altitude increments computed for each acceleration segment at standard conditions are utilized for segment computations at non-standard conditions. In fact, the altitude Above Ground Level (AGL) at the end point of each segment is the same for the non-standard and standard profiles. However, for the non-standard case, the ground roll length of the takeoff segment and the flight angles of the airborne segments are modified in response to the user-defined airport conditions using the equations described below. The non-standard computations are achieved by: (1) an introduction of a specially developed routine for computation of atmospheric coefficients at a given altitude MSL as a function of the airport temperature and elevation; and (2) development of a routine for the automated adjustment of the rateof-climb for acceleration segments due to atmospheric conditions. With the atmospheric coefficients and the rates-of-climb controlled by the user-defined airport elevation and temperature, the SAE equations remain intact.

The takeoff profile generator has been tested for non-standard temperatures from -10 to 100°F and airport elevations up to 6000 ft MSL. Accordingly, the third section of this Appendix presents a set of tables which summarize the runway requirements and operational boundaries of the takeoff profile generator for various combinations of airport elevation and temperature (Tables B-1 through B-9).

## B.1 Standard Conditions (15°C, Zero ft MSL)

This section describes the computation of a standard-condition takeoff profile on a segment-by-segment basis. The Subscripts 1 and 2 refer to the beginning and end of the segment, respectively. The following definitions, constants, and ratios apply to all computations described herein:

Gravitational Constant: g = 32.17

Thermal Gas Constant:  $R_c = 1716.2$ 

Temperature Lapse Rate:  $L \approx 0.003566$  °F/ft or °R/ft

Standard Temperature, °F:  $T_{fap} = T_{f0} = 59.0$ 

Standard Temperature, °C:  $T_{cap} = T_{c0} = 15.0$ 

Standard Temperature,  $^{\circ}R$ :  $T_{rap} = T_{r0} = 518.67$ 

Temperature Ratio: THETA =  $1-[(L)(H_x)/T_{ro}]$ , where  $H_x$  is the

altitude MSL for segment

point X

Pressure Ratio: DELTA = THETA<sup>[g/((Rc) (L))]</sup>

Density Ratio: SIGMA = THETA(g/(Rc)(L))-1

Airport Elevation MSL:  $H_{ap} = 0.0 \text{ ft}$ 

Brake Release Gross Weight = W

Number of Engines supplying Thrust = N

## GROUND ROLL SEGMENT

For the ground roll segment the following apply:

Airport Temperature:  $T_{c1} = T_{c2} = T_{cap}$ 

Pressure

Altitude MSL:  $H_1 = H_2 = H_{ap}$ 

Initial Calibrated

Airspeed:  $V_{c1} = 16.0 \text{ kts}$ 

Given the above, the remaining parameters for the ground roll segment are computed as follows:

Initial Thrust:  $Th_1 = E + F(V_{e1}) + G_1(H_1) + G_2(H_1)^2 + H(T_{e1})$ 

Final Calibrated

Airspeed:  $V_{c2} = (C)(W)^{\frac{1}{2}}$ 

Final Airplane

True Speed:  $V_{t2} = V_{c2}/(SIGMA)^{x}$ 

Final Thrust:  $Th_2 = E + F(V_{c2}) + G_1(H_2) + G_2(H_2)^2 + H(T_{c2})$ 

Segment Horizontal

Length:  $S_g = [(B) (THETA) (W/DELTA)^2]/[(N) Th_2]$ 

where E, F, G<sub>1</sub>, G<sub>2</sub>, and H are engine-dependent coefficients from Data Base Number 11 for maximum takeoff thrust mode;

C is a coefficient from Data Base Number 11 which is appropriate to the takeoff flap/slat setting;

B is a coefficient from Data Base Number 11 which is appropriate to a specific airplane/flap-deflection combination, and varies only with the takeoff flap/slat setting; and

SIGMA, THETA, and DELTA, defined above, are constants equal to 1 at sea level.

## CLIMB SEGMENT

For climb segments the following apply:

Initial Calibrated

Airspeed:  $V_{c1} = V_{c2}$  of the previous segment

Final Calibrated

Airspeed:  $V_{c2} = V_{c1}$ 

Initial Thrust:  $Th_1 = Th_2$  of the previous segment

Initial Temperature:  $T_{c1} = T_{c2}$  of the previous segment

Initial Pressure

Altitude MSL:  $H_1 = H_2$  of the previous segment

Final Segment

Altitude AGL: Altend = As specified in the standard

flight proced: e

Given the above, the remaining parameters for the climb segment are computed as follows:

Final Segment

Altitude MSL: H<sub>2</sub> = Alt<sub>end</sub> + H<sub>ap</sub>

Average Segment

Altitude:  $H_{avg} = 0.5(H_1 + H_2)$ 

Final Segment

Temperature:  $T_{c2} = [(T_{fap} - L(H_2)) - 32](5/9)$ 

Average Segment

Temperature:  $T_{cavg} = [(T_{tap} - L(H_{avg})) - 32](5/9)$ 

Average Calibrated

Airspeed:  $V_{cavg} = V_{c1} = V_{c2}$ 

Average Segment

Thrust:  $Th_{avg} = E + F(V_{cavg}) + G_1(H_{avg}) + G_2(H_{avg})^2 + H(T_{cavg})$ 

Average Airplane

Weight:  $W_{avg} = W/\{[THETA]^{(g/((Rc)(L)))}\}$ 

Sine of the

Flight Angle:  $SIN_{acq} = k\{[(N)(Th_{avg}/W_{avg})] - R\}$ 

where k = 1.01 for  $V_{cavg} \le 200$ ; and

 $= 0.95 \text{ for } V_{cavg} > 200$ 

Cosine of the

Flight Angle:  $COS_{ang} = (1 - SIN_{ang}^2)^{\frac{1}{4}}$ 

Horizontal Segment

Distance:  $S_g = (H_2 - H_1)/(SIN_{ang}/COS_{ang})$ 

Final Segment

Thrust: Th, = E + F( $V_{c2}$ ) + G<sub>1</sub>( $H_2$ ) + G<sub>2</sub>( $H_3$ )<sup>2</sup> + H( $T_{c2}$ )

Final True

Speed:  $V_{t2} = V_{c2}/(SIGMA)^{\kappa}$ 

where E, F, G<sub>1</sub>, G<sub>2</sub>, and H are engine-dependent coefficients from Data

Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

R is a coefficient from Data Base Number 11 which is the nondimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

# ACCELERATION SEGMENT

For acceleration segments the following apply:

Initial Calibrated Airspeed:	$v_{e_1}$	=	V <sub>c2</sub> of the previous segment
Initial Airplane True Speed:	$V_{t1}$	•	V <sub>t2</sub> of the previous segment
Initial Thrust:	$\mathtt{Th}_1$	*	Th, of the previous segment
Initial Temperature:	Ţ <sub>c1</sub>	=	$T_{c2}$ of the previous segment
Initial Pressure Altitude MSL:	H <sub>1</sub>	•	H <sub>2</sub> of the previous segment
Final Calibrated Airspeed:	Ve2	=	As specified in the standard flight procedure
Rate-of-Climb:	$V_{tx}$	•	As specified in the standard flight procedure

Given the above, computation of the remaining parameters is performed using an iterative procedure to arrive at the altitude increment, DelH. If the difference between DelH and DelH<sub>c</sub> (the computed altitude increment for the current iteration) is greater than one ft, DelH is set equal to DelH<sub>c</sub>, and the iterative process is repeated until a difference of one ft or less is achieved.

Initial Assumed		
Altitude Increment:	DelH =	250 ft

# Start of Iterative Loop:

Start of Iterativ	ve Loop	<u>)</u> :	
Final Segment Altitude MSL:	H <sub>2</sub>	#	H <sub>1</sub> + DelH
Final Segment Temperature:	T <sub>c2</sub>	=	${[T_{fap} - L(H_2)] - 32}(5/9)$
Final True Speed:	$V_{t2}$	=	V <sub>c2</sub> /(SIGMA) <sup>%</sup>
Final Segment Thrust:	Th <sub>2</sub>	=	$E + F(V_{c2}) + G_1(H_2) + G_2(H_2)^2 + H(T_{c2})$
Average Segment Thrust:	Th <sub>avg</sub>	=	0.5(Th <sub>1</sub> + Th <sub>2</sub> )
Average. True Speed:	V <sub>tavy</sub>		0.5 (V <sub>t1</sub> + V <sub>t2</sub> )

Average Segment

Altitude:  $H_{avg} = H_1 + 0.5DelH$ 

Average Airplane

Weight:  $W_{avg} = W/\{[THETA]^{[g/(Rc)(L))}\}$ 

Sine of the

Flight Angle:  $SIN_{ang} = V_{tz}/(101.2686V_{tavg})$ 

Flight Angle: GAMMA = arcsin(SIN<sub>ang</sub>)

Horizontal Segment  $0.042062 (V_{t2}^2 - V_{t1}^2)$ 

Distance:  $S_g = \frac{1}{[(N)(Th_{avg})/W_{avg}] - R_{avg} - SIN_{apg}}$ 

Computed Altitude

Increment:  $DelH_c = S_g[tan(GAMMA)](1/0.95)$ 

Deviation of the Computed Altitude Increment from the Altitude Increment Assumed at the Start of the Current

Iteration Cycle DEV =

abs[DelH<sub>c</sub> - DelH]

At this point the status of the iterative process is checked. If DEV is less than 1 ft, then the iterative process is complete. Otherwise,

Altitude

Increment: DelH = DelH<sub>c</sub>

and the iterative process is repeated as above.

where E, F,  $G_1$ ,  $G_2$ , and H are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

 $R_{\rm avg}$  is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

## THRUST REDUCTION SEGMENT

A thrust reduction segment of 1000 ft (horizontal distance) is introduced to allow for a smooth transition of the thrust associated with the Federal Aviation Regulations, Part 36 thrust cutback point. This segment replaces the first 1000 ft of horizontal distance of the next segment which may be either a climb or an acceleration segment. Computation of the parameters associated with the thrust reduction segment and the next segment is performed simultaneously. For the thrust reduction segment the following apply:

Initial Calibrated

Airspeed:  $V_{c1} = V_{c2}$  of the previous segment

Initial Pressure

Altitude MSL:  $H_1 = H_2$  of the previous segment

Initial Temperature:  $T_{c1} = T_{c2}$  of the previous segment

Initial Thrust:  $Th_{ri} = Th_{i}$  of the previous segment

Initial Airplane

True Speed:  $V_{t1} = V_{t2}$  of the previous segment

Horizontal Distance of the

Thrust Reduction Segment:  $S_r = 1000 \text{ ft}$ 

Given the above, the final thrust for the cutback segment is computed as follows:

Thrust:  $Th_{r2} = E + F(V_{c1}) + G_1(A_1) + G_2(H_1)^2 + H(T_{c1})$ 

where E, F, G1, G2, and H are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure.

## Thrust Reduction Followed by an Acceleration Segment:

When the thrust reduction segment is followed by an acceleration segment, the initial thrust of the acceleration segment is set equal to  $\mathrm{Th}_{r2}$  and computation of the remaining parameters associated with the acceleration segment is performed as described previously. The remaining parameters of the thrust reduction segment are computed as follows and the thrust reduction segment replaces the first 1000 ft of the acceleration segment:

True Speed at the end of the thrust reduction

segment:  $V_{tr2} = V_{t1} + (V_{t2} - V_{t1}) (1000/S_g)$ 

Segment Altitude MSL at the end of the thrust reduction

segment:  $H_{r2} = H_1 + DelH(1000/S_g)$ 

where  $V_{\text{t2}}$ ,  $S_{\text{g}}$ , and DelH are parameters computed above for an acceleration segment.

## Thrust Reduction Followed by a Climb Segment:

When the thrust reduction segment is followed by a climb segment, the initial thrust of the climb segment is set equal to  $\mathrm{Th}_{r2}$  and computation of the remaining parameters associated with the climb segment is performed as described previously. The remaining parameters for the thrust reduction segment are computed as follows and the thrust reduction segment replaces the first 1000 ft of the climb segment:

True Speed at the end of the thrust reduction

 $segment: V_{tr} = V_{t1} = V_{t2}$ 

Segment Altitude MSL at the end of the thrust reduction

segment:  $H_r = H_1 + (H_2 - H_1) (1000/S_q)$ 

where  $V_{t2}$ ,  $H_2$  and  $S_q$  are parameters computed above for a climb segment.

#### EXCEPTIONS

The above computations assume the airplane is jet-powered and that the required thrust computations are performed in lbs-thrust. However, if the airplane is propeller-powered the following parameters are factored into the above computations: (1) propeller efficiency and installed net propulsive power for maximum takeoff thrust; and (2) propeller efficiency and installed net propulsive power for maximum climb thrust. In addition, for a select few airplanes, the thrust for a particular segment is given in the standard flight procedure as fixed and as such is not computed by the takeoff profile generator. Finally, for airplanes in Data Base Number 11 for which thrust is expressed in percent-RPM, an intermediate computation is performed to convert to lbs-thrust.

## B.2 Non-Standard Conditions

This section describes the computation of a non-standard-condition takeoff profile on a segment-by-segment basis. Non-standard conditions exist when either the airport elevation is not zero ft MSL and/or the airport temperature is not standard at the airport elevation. The following definitions, constants, and ratios, based upon the concept of density altitude, supplement those described for standard conditions and apply to all computations described herein:

Gravitational Constant:	g	=	32.17
Thermal Gas Constant:	$R_c$	=	1716.2
Temperature Lapse Rate:	L	=	0.003566 °F/ft or °R/ft
Airport Elevation MSL:	$H_{ap}$	=	User-defined in ft
Non-Standard Temperature at Airport Elevation:	$T_{\rm fap}$	=	User-defined degrees F
Standard Temperature, °R:	Tro	=	518.67
Standard Temperature Lapsed to Airport Elevation, °R:	$T_{rap}$	=	Tro - (L) (H <sub>ap</sub> )
Temperature at Altitude, °R:	Tr	=	$T_{rap}$ - [(L)( $H_x$ - $H_{ap}$ )]; where $H_x$ is the altitude MSL for segment point X
Standard Air Pressure:	$\mathbf{P_0}$	=	2116
Standard Air Pressure at Altitude:	P	=	(P <sub>0</sub> ) (DELTA)
Standard Air Density:	$R_0$	=	0.002328
Air Density at Altitude:	R	=	P/[(R <sub>c</sub> )(T <sub>r</sub> )]
Non-Standard Density Ratio:	SIGMA <sub>ns</sub> =		R/R <sub>o</sub>

Non-Standard

SIGMA\_\_\_(1/(g/((Rc)(L)-1))) Temperature Ratio: THETA<sub>na</sub>=

Non-Standard

THETA\_= {g/[(Rc)(L)]} Pressure Ratio: DELTA\_=

## GROUND ROLL SEGMENT

For the ground roll segment the following apply:

Airport Temperature: Tc1  $T_{c2} = (T_{fap} - 32)(5/9)$ 

Pressure Altitude MSL: H, H<sub>2</sub> = Hap

Initial Calibrated

V<sub>c1</sub> = 16.0 kts Airspeed:

Given the above, the remaining parameters for the ground roll segment under non-standard conditions are computed as in Section B.1, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

#### CLIMB SEGMENT

The parameters for the climb segment under non-standard conditions are computed as in Section B.1, Standard Conditions, using the nonstandard THETA, SIGMA, and DELTA, as appropriate.

#### ACCELERATION SEGMENT

With the exception of the iterative process described below, the parameters for the acceleration segment under non-standard conditions are computed as in Section B.1, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

Computation of the remaining parameters is performed using an iterative procedure to arrive at the horizontal distance of the segment,  $S_{gns}$ . If the difference between  $S_{gns}$  and  $S_{qc}$  (the computed horizontal distance for the current iteration) is greater than ten ft,  $S_{gns}$  is set equal to the arithmetic average of  $S_{gns}$  and  $S_{gc}$ , and the iterative process is repeated until a difference of ten ft or less is achieved.

Initial Assumed

 $S_{gns}$ Horizontal Distance: S, computed for standard

conditions

The equations for the acceleration segment under standard conditions are used to supplement the following non-standard computations:

#### Start of Iterative Loop:

Tangent of the

Flight Angle:  $TAN_{ang} = 0.95 (DelH/S_{gns})$  Sine of the

Flight Angle: SIN<sub>ang</sub>= sin[arctan(TAN<sub>ang</sub>)]

Computed Horizontal

Distance:

$$= \frac{(\frac{1}{2}g) (0.95) (V_{t2}^2 - V_{t1}^2)}{[N (Th_{avg})] - R_{avg} - SIN_{ang}}$$

Deviation of the Computed Horizontal Distance from the Horizontal Distance Assumed at the Start of the Current

Iteration Cycle: DEV = abs[S<sub>ec</sub> - S<sub>gns</sub>]

At this point the status of the iterative process is checked. If DEV is less than ten ft, then the iterative process is complete. Otherwise,

Horizontal Distance:

$$S_{gns} = 0.5[S_{gc} + S_{gns}]$$

and the iterative process is repeated as above.

where E, F,  $G_1$ ,  $G_2$ , and H are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

 $R_{\rm avg}$  is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

#### THRUST REDUCTION SEGMENT

The parameters for the thrust reduction segment under non-standard conditions are computed as in Section B.1, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

#### ERROR CHECKING

The non-standard portion of the profile generator maintains several built-in error checks which guard against the computation of improper takeoff profiles. Computation of takeoff profiles is not performed if any of the following conditions are detected:

- (1) the computed flight angle for a climb segment is zero or negative;
- (2) the computed horizontal distance for an acceleration segment is zero or negative;
- (3) the number of iterations required to compute the horizontal distance of an acceleration segment exceeds five hundred; and

(4) the length of the computed ground roll segment exceeds the length of the runway by more than ten percent; if the computed segment exceeds the runway length by less than ten percent, the user is warned of the discrepancy as discussed in Section 2.1.

#### EXCEPTIONS

The exceptions noted in Section 2.1, Standard Conditions, also apply for non-standard conditions.

## B.3 Runway Requirements/Operational Boundaries

Tables B-1 through B-9 present the length (ft) of the ground roll segment computed by the profile generator for all INM airplanes and stage weights. These tables are intended to give the user guidance on the operational boundaries and runway requirements of the profile generator for various airport temperatures, elevations, and runway lengths. These data are presented for nine combinations of airport elevation and temperature intended to cover the range of average yearly conditions at airports across the United States. Tables B-1 through B-3 present these data for 0 ft Above Mean Sea Level (MSL) elevation and three temperatures, 59°F, 40°F and 80°F, respectively. Tables B-4 through B-6 present these data for 3000 ft MSL elevation and three temperatures, 59°F, 40°F and 80°F, respectively. Tables B-7 through B-9 present these data for 6000 ft MSL elevation and three temperatures, 59°F, 40°F and 80°F, respectively. When the generator determines that a profile can not be computed, as discussed in Section B.2, Error Checking, a zero is inserted in the table, e.g., Table B-2, INM Airplane Number 71, Stage Weight 3.

TABLE 8-1: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 0 FT MSL

<u> </u>	<u> </u>			STAGE WEIGHT			
2304 S	1	2	3	•	5	6	7
1	4358	4732	5223	5942	7545	7768	
	4624	5004	5400	6352	7630	9173	10579
	3719	4057	4501	5067	6644	6871	
	2616	2926	3240	3752	4503	5309	6699
5	3846	4157	4481	5257	6297	7545	8679
		4671	5438	6551	8036	9433	
7	4193	4429	5176	6263	7767	8547	
	2721	3109	3523	4193	4671		
,	3279	3739	4160	4913	5992	7186	8040
		3128	3656	4424	5486	6037	
10	2799	3034	3405	4006	4436		
11	2684	3338	3879	4666	\$754	6709	
12	3000	4054	4607	5400	6483	7189	8167
13	3705	<u> </u>	<del></del>	4956	5969	6660	7614
14	2257	3684	4294			<del></del>	
15	2693	3335	3959	4913	5992	7186	
16	3279	3739	4160			7180	4040
17	370\$	4054	4607	3400	6413	<del></del>	8167
18	6967	6967	4943	8556 5828	9799 6813	9799	
19	3997	4369	4943			7868	
20	3371	3656	3954	4609	\$534	6575	7799
21	4669	5071	5463	6353	7614	9032	10657
22	5052	5363	5900	6443	7610	8883	
23	4611	4897	5343	\$811	6741	7747	8869
24	5964	6863	7821	8843			
25	4513	5004	5522	6146			
26	5460	6050	6913	8098	9476		
27	5979	6964	8029	9074			
26	4513	5004	5522	6146			•••
29	5460	6050	6913	\$098	9476		•••
30	5263	6120	6965	7699			
31	3352	3846	4285	5206	6369	ļ	
32	3414	3703	4015	4587	5362	6268	6811
33	3020	3274	3549	4062	4765	5576	5970
34	3067	3467	3924	4411	5328	6299	
35	3506	3981	4489	5506			•••
36	3167	3681	4135	5041			
37	4221	4827	5609				•••
38	3292	4035					
39	3184	3746	4612				
40	3634	4416	5227			***	
41	2124	2638	3133				
42	3075	3310	3893	4618		<u> </u>	
43	3634	4416	5227				
44	2124	2638	3133				
45	3075	3310	3893	4618			
46	3653	4186	4839	•			
47	3303	3688	4096	4526	•••		
48	3897	4708	5601				
49	3685	4155	4728	5991			
50	4002	4548	5131	6493			
51	2646	2846	3091	3573	4217		
52	2747	2960	3219	3692	4376	512)	
\$3	2826				•••		•••
54	2569						
55	3609						

TABLE B-1: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 0 FT MSL (CONTINUED)

	<u> </u>			STAGE WEIGHT								
IME #	1	1 2	3	T	5	•	7					
54	4136											
\$7	3130											
50	3498			<del> </del>	<del> </del>							
57	3725											
60	2972			<del> </del>								
61	4945											
62	3896			<del></del>								
63	2697	1397	4586									
64	1794						•••					
63	1211		<del></del>	<del> </del>	•••							
66	3860	4921	5483	† <del></del>		•						
67	2639			<del> </del>								
60	2560			<del> </del>								
65	1239		<del> </del>	<del> </del>								
70	3181	4261	5396									
71	1520	1856	2234	<del></del>	•••							
72	1792	2332		<del> </del>			•••					
73	2082		<del>                                     </del>	<del> </del>								
74	632		<del> </del>	<del> </del>								
75	738		<del>                                     </del>	<del> </del>								
76	1584	<del>                                     </del>	<del> </del>	<del></del>								
<del></del>	699			<del> </del>								
78	10532		<del>                                     </del>	<del> </del>								
79	4153	6477		<del> </del>								
80	\$158	7065		<del> </del>								
61	4505	6732		<del> </del>								
62	\$120	7651		<del></del>								
#3	3768	4193	4551	5313	6355	7861	9137					
64	4084	4421	4756	5590	6711	8052	9291					
85	3657	4252	4730	5769								
86	3569	4125	4636	5657		•••						
87	2753	2985	3237	3700	4351	5096	5457					
44	2942	3608	4350	<del></del>								
89	3324	4085	4821									
90	3187	3894	4678	<del>                                     </del>								
91	11242											
92	9308		<del></del>	<del></del>								
93	3244	3596	4111	4820	5645							
94	3004	3331	3676	4092								
95	3062											
36	4190					<del></del>						
97	3640	4331	5158	5984								
98	4136			3700								
**	2427	<del></del>				\ <del></del>						
100	4513	5004	5522	6146								
100	5460	6050	6913	8098	9476							
102	3968	4287	4619	5445	6343	7459	8831					
		4543	<del></del>	<del> </del>		<del></del>	<del></del>					
103	4202	4543	4899	5784	6749	7950	9430					
104	3000		<del>}</del>	<del>                                     </del>								
105	3000											
	3000			1								
107	3000			<del> </del>								

TABLE 8-2: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F, ELEVATION 0 FT MSL

5 7545 7020 6112 4142 5793 8098 7767 4671 5512 5486 4081 5294 5964 5510 5512 5964 9015 6268 5091 7005	6 7788 8439 6322 4884 6942 9433 8547  6611 6037  6172 6606 6127  6411 6606 9015 7239	7 9733 6163 7984 7984 7984 7984 7984 7534 7634 7534 7005 7434 7534 .
7545 7020 6112 4142 5793 8098 7767 4671 5512 5486 4081 5294 5964 5510 5512 5964 9015 6268	7788 8439 6322 4884 6942 9433 8547 6611 6037 6172 6606 6127 6611 6606 9015 7239	7514 7514
7020 6112 4142 5793 8098 7767 4671 5512 5486 4081 5294 5964 5510 5512 5964 9015 6268	8439 6322 4884 6942 9433 8547 6611 6037 6172 6606 6127 6611 6606 9015 7239	9733 6163 7986 7436 7514 7005 7434 7514
6112 6142 5793 8098 7767 4671 5512 5486 4081 5294 5964 5510  5512 5964 9015 6268	6322 4884 6942 9433 8547  6611 6037  6172 6606 6127  6611 6606 9015 7239	7984 7984 7434 7534 7005 7434 7514
4142 5793 8098 7767 4671 5512 5486 4081 5294 5964 5510  5512 5964 9015 6268 5091	4884 6942 9433 8547  6611 6037  6172 6606 6127  6611 6606 9015 7239	7984 7984 7434 7434 751
5793 8098 7767 4671 5512 5486 4081 5294 5964 5510 5512 5964 9015 6268	6942 9433 8547 6611 6037 6172 6606 6127 6611 6606 9015 7239	7984 7434 7514 7005 7434 7514
8098 7767 4671 5512 5486 4081 5294 5964 5510  5512 5964 9015 6268 5091	\$433 \$547  6611 6037  6172 6606 6127  6611 6606 9015 7239	7434  7514 7005  7434 7514
7767 4671 5512 5486 4081 5294 5964 5510 5512 5964 9015 6268	8547  6611 6037  6172 6606 6127  6611 6606 9015 7239	7434  7514 7005  7514 
4671 5512 5486 4081 5294 5964 5510  5512 5964 9015 6268 5091	6611 6037  6172 6606 6127  6611 6606 9015	7434  7514 7005  7434 7514
5512 5486 4081 5294 5964 5510  5512 5964 9015 6268 5091	6611 6037  6172 6606 6127  6611 6606 9015	7436  7514 7005  7434 7514
5486 4081 5294 5964 5510  5512 5964 9015 6268 5091	6037  6172 6606 6127  6611 6606 9015 7239	7514 7005  7414 7514
4081 5294 5964 5510  5512 5964 9015 6268 5091	6172 6606 6127  6611 6606 9015	7514 7005  7414 7514
5294 5964 5510  5512 5964 9015 6268	6172 6606 6127  6611 6606 9015 7239	7514 7005  7414 7514
5964 5510  5512 5964 9015 6268 5091	6606 6127  6611 6606 9015 7239	7514 7005  7414 7514
5510  5512 5964 9015 6268 5091	6127  6611 6606 9015 7239	7005  7414 7514
5512 5964 9015 6268	 6611 6606 9015 7239	7634 7514
5512 5964 9015 6268 5091	6611 6606 9015 7239	7434 7514
5964 9015 6268 5091	6606 9015 7239	7514
9015 6268 5091	9015 7239	
6268 5091	7239	
5091	<del></del>	
	6049	
7005		7175
	8309	9804
7001	6172	
6202	7127	8159
		***
8718		
8718		
5860		•••
4933	5767	6266
4394	5130	5492
4902	5795	
		•••
•••		
		<del></del>
	ļ	
	ļ	
	5718 8718 8718 5960 4933 4384 4902	### ##################################

TABLE B-2: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F, ELEVATION 0 FT MSL (CONTINUED)

<u> </u>	STAGE WEIGHT								
2304 6	1	2	3	T .	5	6	7		
	<del></del>	<del></del>	<del> </del>	<del>                                     </del>					
37	2880	<del> </del>		<del> </del>					
30	3210								
39	3427								
60	2734		<del>                                     </del>	<del> </del>					
61	4550				<del></del>				
62	3586	<del>                                     </del>	<del> </del>	<del> </del>					
63	2435	3068	4141	<del></del>	•••				
66	1651			<del></del>					
65	1093	<del></del>	<del> </del>	<del></del>					
66	3485	4443	5312	<del> </del>					
67	2362			<del> </del>					
	2311	<del></del>							
- 66	<del></del>	<del> </del>	<del></del>	<del></del>					
70	2873	3794	4872						
	1372	1676	10/2						
72	1572	2106							
72	1618	2106							
	<del></del>								
74	570				<del></del>				
75	667	<del>                                     </del>				<del></del>			
76	1431								
78	9689								
	<del> </del>								
79	3820	5954	<del></del>						
80	4746	6500							
81	4068	6079	•••			<del></del>	<del></del>		
82	4624	3838	41.00	4888	5847	7232	8406		
63	3467	4967	4376	5143	6174	7408	8547		
84	<del> </del>	3912	4352	5307					
05 06	3364	3795	4265	5204		<del></del>			
87	2533	2746	2978	3411	4002	4688	5020		
89	2707	3326	4002						
89	3058	3758	4435				<del>                                     </del>		
90	2932	3583	4304				<del>                                     </del>		
91	10327			<del>                                     </del>					
92	8563								
93	2984	3308	3782	4434	5194				
94	2764	3065	3382	3764					
95	2817				<del> </del>	<del> </del>			
96	3855			<del> </del>					
97	3349	3985	4745	5505		<del> </del>			
98	3805								
99	2233								
100	4513	5004	5522	6146		<del></del>			
101	5460	6050	6913	8098	9476		<del>                                     </del>		
102	3369	3639	3920	4618	5378	6321	7479		
103	3501	3784	4079	4812	5611	6605	7827		
104	3000								
105	3000			<del>                                     </del>	<del> </del>	<del> </del>			
106	3000	<del>                                     </del>							
	<u> </u>	<del>                                     </del>		<del></del>		<del></del>			
107	3000			<u></u>	<u> </u>	<u> </u>			

TABLE B-3: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 80°F , ELEVATION 0 FT MSL

	T	·		STAGE WEIGHT			
E304 #	1	2	3		5	6	7
1	4358	4732	5223	5842	7545	7788	
	3053	3468	5901	6941	0330	10024	11561
<del></del>	4064	4433	4919	5537	7260	7509	
<del></del>	2058	3198	3541	4100	4920	5001	7321
	<del> </del>		4896	5745	6081	8245	9484
	4202	4542		<del> </del>	<del></del>		
	4193	4671	5434	6263	7767	9433 8547	
<del></del>	3963	4429	5176	<del></del>	<del></del>		
•	2721	3109	3523	4193	4671	***	
•	3583	4086	4545	5369	6548	7852	8630
10	2799	3128	3656	4424	5486	6037	
	2933	3315	3721	4378	4847		***
12	3278	3647	4239	5099	6288	7332	
13	4049	4430	5034	5901	7084	7846	8925
14	3668	4025	4594	5415	6544	7277	8350
15	2943	3644	4326			•••	
16	3583	4086	4545	5369	6548	7852	8830
17	4049	4430	5034	5901	7084	7846	<b>#925</b>
18	7614	7614	9350	9350	10708	19708	•••
19	4368	4797	5401	6380	7445	8598	
20	3683	3995	4321	5037	6047	7185	8523
21	5102	5542	5970	6942	8321	9870	11546
22	5521	5882	6447	7041	<b>8</b> 315	9707	•••
23	\$039	\$351	5839	6350	7366	8465	9692
24	5968	6463	7821	8841		**-	•••
25	4932	5468	6034	6716		-1-	
26	5967	6612	7554	8849	19355		
27	6533	7610	8773	9915			•••
28	4932	5468	6034	6716		•	
29	5967	6612	7554	8849	10355		
30	\$751	6688	7611	8413			
31	3663	4203	4683	5689	6960	***	
32	3731	4047	4387	5012	3860	6850	7443
33	3300	3578	3878	4439	5207	6094	6524
34	3352	3788	4287	4820	5823	6883	
35	3832	4351	4905	6016		•••	
36	3488	4029	4526	5518			
37	4613	5274	6129				
38	3598	4409					•••
39	3480	4093	5040				
40	3971	4825	5712				
41	2321	288)	3424				
42	3361	3617	4254	5047	<del> </del>		
43	3971	4825	5712			<del></del>	
	<b></b>		<del></del>	<u> </u>			<del></del>
-44	2321	2883 3617	3424 4254	5047			
45	3361	<del></del>	<del> </del>	<del></del>		<u> </u>	
	3992	4574	5288	1246	<del> </del>		
47	3609	4030	6476	4946	•••		
48	4258	5145	6121				
	4027	4540	5166	6547			
49	1	4970	5607	7095			
50	4373						
	4373 2891	3111	3377	3904	4600		
50	<del></del>		3377 3519	3904 4036	4608 4783	\$600	
50	2891	3111	<del> </del>		<del> </del>		
50 52 52	2891 3002	3111 3236	3519	4036	4783	\$600	

TABLE B-3: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 80°F , ELEVATION 0 FT MSL (CONTINUED)

		<del></del>	<del> </del>	STAGE WEIGHT			
2301 0	1	2	3	4	5	6	7
56	4136			· · · · · · · · · · · · · · · · · · ·			
\$7	3421						
30	3#23						
59	4071						
60	3248						
61	5404						
62	4260					•••	
63	3006	3787	5111				
64	1961						
65	135						
66	4302	5485	6558				<del> </del>
67	2941						
68	2853		<del> </del>	<del></del>			
69	1361	<del></del>		<del></del>			<del> </del>
70	3546	4683	6014				<del></del>
71	1694	2069	,				
72	1997	2599					
73	2321						
74	704	<b></b>			ļ		
75	823		<del></del>			***	•••
76	1766					•••	
77	780					***	[
78	11509					•••	
79	4538	7077					
*0	5637	7720			•••		•••
#1	5022	7504					
82	5707	8528					ļ
83	4118	4582	4973	5406	6945	8590	9984
**	4463	4031	5197	6109	7334	8799	10152
85	3996	4646	5169	6304			
96	3901	4508	3066	6182		•••	•••
87	3009	3262	3537	4052	4754	5569	5963
**	3215	3943	4754				
89	3633	4464	5268	***	•••		
90	3483	4255	\$112				
91	12306						
92				•••			
93	10171			•••	***	•••	
			<del></del>				
94	10171	•••		•••	•••	•••	
94 95	10171 3544	3929	4493	5267	6169	•••	
	10171 3544 3283	3929 3640	4493 4017	5267 4472	6169	•••	
95	10171 3544 3283 3346	3929 3640	4493	5267 4472	6169		
95 96	10171 3544 3283 3346 4579	3929 3640	4493 4017	5267 4472	6169		
95 96 97	10171 3544 3203 3346 4579 3978	3929 3640  4733	4493 4017  5637	5267 4472  6539	6169 		
95 96 97 98	10171 3544 3283 3346 4579 3978 4520	3929 3640  4733	4493 4017  5637	5267 4472  6539			
95 96 97 98 99	10171 3544 3203 3346 4579 3978 4520 2652	3929 3640  4733	4493 4017  5617	5267 4472  6539			
95 96 97 98 99 100	10171 3544 3203 3346 4579 3978 4520 2652 4513	3929 3640  4733  5004	4493 4017  5637  5522	5267 4472  6539  6146			
95 96 97 98 99 100	10171 3544 3203 3346 4579 3978 4520 2652 4513 5460	3929 3640  4733  5004 6050	4493 4017  5637  5522 6913	5267 4472  6539  6146	6169      9476		
95 96 97 98 99 100 101	10171 3544 3283 3346 4579 3978 4520 2652 4513 5460	3929 3640  4733  5004 6050	4493 4017  5637  5522 6913 5564	5267 4472  6539  6146 8098 6563	 6169      9476 7651		10667
95 96 97 98 99 100 101 102 103	10171 3544 3283 3346 4579 3978 4520 2652 4513 5460 4777 5189	3929 3640  4733  5004 6050 5163	4493 4017  5637  5522 6911 5564 6055	5267 4472  6539  6146 8098 6563 7156	6169 9476 7651 8356		10667 11708
95 96 97 98 99 100 101 102 103 104	10171 3544 3283 3346 4579 3978 4520 2652 4513 5460 4777 5189	3929 3640  4733  5004 6050 5163	4493 4017  5637  5522 6913 5564 6055	5267 4472  6539  6146 8098 6563 7156	6169 9476 7651 8358	9004 9858	10667 11708

TABLE B-4: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 3000 FT MSL

		·· <u>·</u>		STAGE WEIGHT			
2300 0	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	
2	5750	6322	6714	7895	9482	11396	13139
3	4627	5946	5598	6301	6257	8540	
•	3255	3641	4031	4667	5600	6691	8327
•	4693	5069	5464	6409	7673	9191	10569
•	4193	4671	5438	6551	8098	9433	
7	3963	4429	5176	6263	7767	8547	
•	2721	3109	3523	4193	4671		
•	4028	4592	5109	6032	7355	8818	9913
10	2799	3128	3636	4424	5486	6037	
11	3328	3761	4221	4965	5497		
12	3848	4281	4976	5985	7382	8607	
13	4748	5195	5904	6921	6308	9202	10467
16	4136	4537	5177	6101	7371	8195	9367
15	3403	4213	0				
16	4028	4593	5109	6032	7355	8618	9913
17	4748	\$195	5904	4921	8308	9202	19467
10	8684	8684	10661	10661	13208	12206	
19	5160	3666	6381	7537	8797	10160	
20	4130	4479	4844	5645	6775	8047	9543
21	6001	6519	7022	8166	9788	11611	13700
22	6263	6674	7315	7987	9429	11004	
23	5744	6100	6635	7236	8393	9643	11038
24	5964	6863	7821	0041			
25	5823	6457	7125	7930			
26	6755	7485	8551	10015	11716		•••
27	7666	8929	10294	11634			
28	5823	6457	7125	7930			***
29	6755	7485	8551	10015	11718		
30	6521	7582	8629	9537			
31	4324	4961	5528	6716	8216		
32	4196	4550	4933	5634	6585	7695	8360
33	3606	3909	4236	4848	5684	6649	7117
34	3605	4072	4607	5177	6249	7383	
35	4159	4721	5320	6520		•••	***
36	3926	4534	5092	6206			•••
37	5420	6207	7212			***	
38	4081	5000					
39	3965	4663	5741				
40	4651	5651	6690				
41	2712	3360	4001				
42	3957	4259	5009	5943			
43	4651	5651	6690		••-		•••
44	2712	3368	4001			•••	•••
45	3957	4259	5009	5943	•••		
46	4674	5355	6191				
47	4094	4571	5076	5608			
40	4795	5792	6889				
49	4548	5128	5834	7391			
\$0	5029	5715	6447	8157			
51	3259	3506	3806	4399	5191		
52	3207	3541	3851	4414	5229	6119	•••
53	3377				•••		
54	32#1						
				·		<b>4</b>	L

TABLE B-4: RUMMAY REQUIF MENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 3000 FT MSL (CONTINUED)

	STAGE WEIGHT								
2304 8	1	2	3	4	5	6	7		
56	4136						•		
57	3647								
58	4240								
59	4790								
60	3458				•••				
61	5994								
62	4798								
63	3261	4100	5545						
64	2156								
65	1464		•••				•••		
66	4667	5951	7115				•••		
67	3191								
68	3095			•	•••	•••			
69	1499								
70	3847	5081	6525						
71	1838	2245	0						
72	2167	2820			***	•••			
73	2518		•••			•••			
74	764								
75	893				***				
76	1916			•••					
77	846								
78	13454								
79	5094	7944					•••		
80	6)28	8663					•••		
61	5448	6141							
62	6192	9252	***	•••					
83	4637	5160	5599	6535	7815	9662	11226		
84	5043	5459	5072	6900	8281	9932	11457		
85	4503	5235	5823	7099					
86	4233	4890	5494	6690		•••			
87	3464	3755	4071	4664	5471	6403	6861		
88	3717	0	0						
69	3949	4849	5718						
90	4009	4896	5881						
91	11820								
92	11445								
93	4029	4466	5106	5985	7008		•••		
94	3800	4214	4650	5176	,,,,,				
95	3660		***						
96	5268								
97	4698	5591	6659	7725					
98	5066	2221	••••	1725					
	3913	•••							
100	4513	5004	5522	6146					
			6913						
101	5460	6050		8098	9476	4116			
102	4968	5367	5783	6816	7939	9335	11051		
103	5183	5603	6041	7131	4316	9796	11616		
104	3000								
105	3000		•••						
106	3000					•••			
107	3000		•••						

TABLE B-5: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F , ELEVATION 3000 FT MSL

	I	· · · · · · · · · · · · · · · · · · ·		STAGE WEIGHT	<del></del>		
tiot e	1	2	3		5	6	7
1	4358	4722	5223	5942	7545	7788	
	<del>                                     </del>	5724	6176	7263	9723	10484	
	5290		<del></del>	5796	7597	7857	12088
	4256 2995	4642 3350	5150 3709	4293	5152	6073	7661
<del></del> _		<del> </del>		5096	7059		
5	4315	4664	5027	<del>}</del>		8456	9723
	4193	4671	5438	6551	8094	9433	
7	3963	4429	5176	6263	7767	8547	
	3721	3109	3523	4193	4671		
<del></del>	3704	4226	4700	5550	6767	8112	9130
10	2799	3138	3656	4424	5486	6037	
11	3062	3460	3884	4568	5057		
12	3540	3939	4578	5506	6791	7918	
13	4364	4780	5432	6367	7643	8466	9630
14	3805	4174	4763	5613	6781	7539	8617
15	3130	3875	0				***
16	3704	4226	4700	5550	6767	8112	9120
17	4364	4740	5432	6367	7643	8466	9430
18	7989	7989	9808	9404	11231	11231	•••
19	4747	5213	\$870	6934	8093	9347	
20	3799	4121	4456	5193	6233	7403	8779
21	5521	5997	6460	7513	9005	10682	12604
22	5764	6140	6729	7348	8675	10124	•••
23	5284	5611	6122	6657	7721	8871	10154
24	5969	6863	7821	8841	•••	•	
25	5357	5940	6554	7295	••-		***
26	6215	6886	7867	9214	19780	•••	•••
27	7052	8215	9470	10703		•••	***
28	5357	5940	6554	7295		•••	•••
29	6215	6886	7867	9214	10780		•••
30	5999	6976	7938	8774			***
31	3978	4564	5086	6179	7560		•••
32	3860	4186	4538	\$283	6058	7079	7691
33	3317	3596	3897	4460	5229	6117	6547
34	3316	3746	4238	4763	5749	6792	
15	3826	4343	4895	5998			
36	3607	4165	4678	5701			
37	4994	5710	6635				***
38	3754	4600		•••			
39	3648	4290	5262				
40	4279	5199	6155	***			
41	2495	3099	3681				
	<del></del>		<del></del>	<del>                                     </del>			
42	3640	3918	4608	5467			
42	<del></del>	<u> </u>		5467			
43	4279 2495	3918 5199 3099	4608 6155 3681	<del></del>			
43	4279 2495	5199 3099	6155 3681				
43	4279 2495 3640	5199 3099 3918	6155 3681 4608	5467			
43 44 45 46	4279 2495 3640 4300	3099 3099 3918 4927	6155 3681 4608 5696	5467		•••	
43 44 45 46 47	4279 2495 3640 4300 3766	5199 3099 3918 4927 4206	6155 3681 4608 5696 4670	\$467  \$160			
43 44 45 46 47 48	4279 2495 2640 4300 3766 4411	5199 3099 3918 4927 4206 5329	6155 3681 4608 5696 4670 6337	\$467  \$160			
43 44 45 46 47 48 49	4279 2495 3640 4300 3766 4411 4184	5199 3099 3918 4927 4206 5329	6155 3681 4608 5696 4670 6337 5367	5467  5160  6799			
43 44 45 46 47 48 49 50	4279 2495 1640 4300 3766 4411 4184 4626	5199 3099 3918 4927 4206 5129 4717 5257	6155 1681 4608 5696 4670 6337 5367 5931	5467  5160  6799 7505			
43 44 45 46 47 48 49 50	4279 2495 1640 4300 3766 4411 4184 4626 2998	5199 3099 3918 4927 4206 5329 4717 5257 3225	6155 3681 4608 5696 4670 6337 5367 5931 3502	5467  5160  6799 7505 4047	4775		
43 44 45 46 47 48 49 50 51	4279 2495 3640 4300 3766 4411 4184 4626 2998 3023	5199 3099 3918 4927 4206 5329 4717 5257 3225	6155 3681 4608 5696 4670 6337 5367 5931 3502 3542	5467  5160  6799 7505 4047 4060	4775 4809		
43 44 45 46 47 48 49 50 51 52 53	4279 2495 2490 2490 3400 4300 3766 4411 4184 4626 2998 3023 3107	5199 3099 3918 4927 4206 5129 4717 5257 3225	6155 3681 4608 5696 4670 6337 5367 5931 3502	5467  5160  6799 7505 4047 4060	4775 4809		
43 44 45 46 47 48 49 50 51	4279 2495 3640 4300 3766 4411 4184 4626 2998 3023	5199 3099 3918 4927 4206 5329 4717 5257 3225	6155 3681 4608 5696 4670 6337 5367 5931 3502 3542	5467  5160  6799 7505 4047 4060	4775 4809		

TABLE 8-5: RUMWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F , ELEVATION 3000 FT MSL (CONTINUED)

				STAGE WEIGHT			
2300 6	1	2	,	•	\$	6	7
*	4136					•••	•
\$7	3355					•••	
54	3901						
59	4407						
60	3101	•••					
61	5514			<u> </u>			
62	4414						
63	2945	3710	5007				
- 64	1983				•••	•••	
	<del> </del>			<del></del>			
-65	1322		ļ <u> </u>				
	4214	5373	6424				
67	2881	•••		•••			
	2795				•		
69	1353			***	•••	•••	***
70	3474	4588	5892			•••	
71	1660	2027	•		•••		
72	1957	2546		•••		•••	•••
73	2274						***
74	690	•••		•••	•••		•••
75	00€						•••
76	1730					•••	•••
77	764						•••
78	12377		•••				•••
79	4686	7308			•••		
80	5822	7972				•••	•••
81	4920	7351					
82	5591	8354					
83	4266	4747	5151	6012	7189	8885	10329
84	4639	5022	5402	6348	7618	9137	10540
45	4143	4816	5357	6531			
86	3695	4499	5054	6162		•••	***
87	3186	3455	3745	4290	5033	5895	6312
11	3420	4193					
49	3633	4461	5261	<del> </del>			
90	3687	4505	5413	<del></del>		•••	
91	12695						
			<del> </del>				
92	10529	4100	4693	<del> </del>	<del> </del>		
93	3706	4108	4697	5506	6448		
94	3496	3877	4278	4762	•••	***	
95	3367		***				
96	4846				•••		
97	4322	5143	6126	7107	•••		
98	4661					•••	
99	2680					•	•••
100	4513	5004	5522	6146			
101	5460	6050	6913	8098	9476		
102	4224	4563	4915	5790	6742	7923	9374
103	4333	4683	5047	5953	6939	8166	9675
104	3000						•••
105	3000						
106	3000		·				

TABLE B-6: RUNNAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE  $80 \, ^{\circ}$ F, ELEVATION 3000 FT MSL

				STAGE VELGET			
2306 6	1	2	1 3	<u> </u>	5	6	7
1	4358	4732	5223	5942	7545	7788	
	4283	6799	7336	\$628	10362	12453	14358
3	5056	5514	6117	6885	9023	9332	
<del></del>	3857	3979	4405	5100	6120	7213	9099
5	5126	5540	5971	7003	#3#5	10044	11549
	4193	4671	5438	6551	8098	9433	
7	3963	4429	5176	6263	7767	8547	<del> </del>
	<del></del>		3523	4193	4671		
*	4402	3109 5020	5583	6592	8037	9636	10833
10	2799	3128	1656	4424	5486	6037	
11	3637	4210	4623	5426	6007		
		4678	5438	6541	8066	9405	
13	4205 5109	5677	6452	7563	9079	10056	11438
		4958	5658	6667	8055	8955	10236
14	4519		<del></del>	<b></b>			
15	3718	5000	0	6592	8037	2676	10013
76	4402	5020	\$583	7563	9079	9636	10033
17	3149	5677	6452		<u> </u>	18056	11436
10	3489	5489	11650	11650	13340	12340	
19	5638	6192	6973	6237	9613	11102	
20	4513	4895	\$293	6168	7403	8794	10420
31	6558	7123	7673	8924	10696	12688	14971
22	6846	7293	7993	8728	10304	12025	•••
23	6277	6665	7272	7908	9171	10537	12062
24	5968	6863	7821	8841			
25	6363	7056	7785	8666			
26	7342	£179	9344	10944	12805		•••
27	8377	9758	11249	12713			•••
	6363	7056	7785	8666			•••
29	7382	8179	9344	10944	12805		
30	7126	8286	9429	10422		•••	
31	4725	5422	6041	7339	8980		
32	4545	4973	5390	6157	7196	8409	9136
33	3940	4272	4629	5297	6211	7265	7777
34	3939	4450	5014	5657	6829	8068	•••
35	4545	\$159	5814	7125		•	
36	4297	4962	5573	6792		•••	
37	5911	6782	7681				
38	4460	5464		***	•-•		
39	4333	5096	6274		•••		
40	5082	6176	7311		•••		•••
41	2964	3681	4372		*	•	•••
42	4324	4654	5473	6494	•••		
43	5082	6176	7311		***		•••
44	2964	3681	4372	•••	••-	•••	
45	4324	4654	5473	6494			
46	3108	5852	6766				•••
47	4473	4995	5547	6129			
44	5240	6330	7528				•••
49	4970	5603	6375	8076	•••		
50	5495	6245	7045	8914			
51	1561	3631	4159	4807	5672		
52	3593	3871	4210	4825	5716	6689	•
53	3690			•••			
54	3586						
	5212						

TABLE 8-6: RUNNAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 80°F , ELEVATION 3000 FT MSL (CONTINUED)

ſ	STAGE MEIGHT								
2304 0	3	2	3	•	s	6	7		
54	4136								
57	3945								
58	4633								
59	5234								
60	3779								
61	6550				•••				
62	5243								
63	3635	4580	6181	···					
64	2356								
65	1632		•••		•••	•••	•••		
66	5203	6633	7930				•••		
67	3556	•••							
60	3450	•••							
69	1676		***	· · · · · ·			•		
70	4289	5663	7273			•••			
71	3049	2502	0	•••	***				
72	3415	3143	***	•••					
73	2807								
74	951						· · · · · ·		
75	995								
76	2136								
77	943								
78	14702				***		•••		
79	5566	8681							
80	6915	9469	***	•••					
61	6473	9074	***						
82	6902	10313							
83	5067	5638	6118	7142	8540	10559	12269		
84	5511	5965	6417	7540	9049	10653	12519		
85	4921	5721	6363	7758					
86	4626	5344	6003	7320			•••		
87	3785	4103	4449	1096	5979	7002	7497		
88	4062	đ	•						
89	4315	5299	6249	*					
90	4380	5351	6427						
91	15127								
92	12506								
92	4402	4880	\$579	6540	7659				
94	4153	4605	5081	5656					
95	3999	•••							
96	5756								
97	5134	6109	7276	8442		•••			
98	5536								
99	3183								
100	4513	5004	5522	6246					
101	5460	6030	6913	8098	9476				
102	5970	6451	6952	8200	9557	11245	13320		
103	6372	6892	7433	8782	10254	12089	14351		
104	3000								
105	3000								
106	3000	•••							
107	3000								

TABLE 8-7: MUNNAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 6000 FT MSL

	STRAGE WEIGHT								
2300 4	1	2	3	1	5	6	7		
	4358	4732	5223	5842	7545	7788			
1			<del></del>	9925	<del></del>	<del> </del>			
3	7231	7823	8441		11917	14319	16507		
3	5819	6346	7039	7922	10380	10735			
•	4096	4581	5072	\$870	7043	6300	10467		
5	\$763	6227	6711	7870	9419	11279	12966		
•	4193	4671	5438	6551	8094	9433	•••		
7	3963	4429	5176	6263	7767	8547			
•	2721	3109	3523	4193	4671				
,	4949	5642	6274	7406	9027	10818	12160		
10	2799	3126	3656	4424	5486	6037	•••		
22	4142	4680	5252	6176	6837				
12	4961	5520	6416	7717	9518	11098			
13	6117	4692	7605	8915	10702	11654	13484		
14	5120	5625	6418	7561	9132	10151	11600		
15	0	0	•	•••					
16	4949	3642	6274	7406	9027	10818	12160		
17	6117	6692	7605	8915	10702	11854	13484		
10	10886	10886	13362	13362	15298	15298			
19	6694	7351	8279	9780	11415	13185	•••		
20	5095	\$525	5974	6961	8352	9918	11750		
21	7753	8422	9072	10550	12646	15002	17702		
22	7807	8316	9112	9948	11741	13698			
23	7189	7634	8326	9054	10499	12061	13863		
24	5968	6863	7821	8841					
25	7483	4294	9156	10191					
26	8729	9671	11049	12942	25242				
27	9952	11592	13365	15105					
- 20	7483	8298	9156	10191					
29	8729	9671	11049	12942	15142				
30	8423	9795	11146	12320					
31	5605	6432	7167	8708	10655				
		<del></del>			<del></del>				
32	5191	5629	6101	6967	8140	9510	10331		
33	4347	4712	5105	5840	6845	8004	8566		
34	4329	4889	5529	6211	7493	8848			
35	4905	\$656	6372	7804	•••				
36	4868	\$620	6311	7689					
37	7016	8023	9323				•••		
38	5089	6235							
39	4966	3849	7188		•••				
40	5983	7270	8607						
41	3481	4323	5135						
42	5121	5512	6483	7692	•••		•••		
43	5983	7270	8607						
44	3481	4323	5135						
45	5121	5512	6483	7692		•••	•••		
46	6011	6887	7962				•••		
47	5288	5905	6557	7245			•••		
48	5939	7173	4529	•••					
49	5650	6368	7245	9176			•••		
50	6354	7220	\$145	10305			•••		
	4040	4346	4718	5451	6431				
51			1	5327	6308	7378			
51 52	3970	4276	4649	,	,				
<del></del>	3970 4103	4276					•••		
52					<del></del>	<del> </del>			

TABLE B-7: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 59°F , ELEVATION 6000 PT MSL (CONTINUED)

	STAGE METGET								
IND #		2	3	4	s	6	,		
56	4136								
\$7	4399								
50	5180								
59	6192	***							
60	4160								
61	7322								
62	6054					•••			
63	3960	4989	6733						
64	2613	<del></del>		•••					
65	1778				•••				
66	\$667	7225	8639						
67	3874					•••			
68	3758								
69	1820								
70	4672	6169	7923		***	•••			
71	2232	2726	•				•		
72	2631	3424							
73	3057								
74	928			<del></del>					
75	1004	<del></del>				***			
76	2327	<del></del>							
77	1027	<del></del>							
78	17276	<del> </del>				•••	<del></del>		
79	6260	9762			•••				
80	7779	10648							
81	4616	9885				•••			
82	7519	11234							
83	5744	6391	6934	0092	9673	11956	11009		
84	6267	6783	7296	8571	10283	12329	14210		
85	5582	6488	7215	8794					
86	5073	5858	6578	1016					
97	4381	4749	5148	5897			8674		
88	- 1362	0	0	3657	6918	8101			
89	4739	5815	6854						
<del></del>			7434						
90	17102	6190		***			•••		
92		<del> </del>							
	14072								
93	5034	5500	6378	7475	<b>\$753</b>				
94	4833	5359	5913	6582	***				
95	4448					•••			
96	6659						***		
97	6095	7253	8639	10023					
98	6323					•••			
99	3528								
100	4513	5004	5522	6146					
101	5460	6050	6913	8098	9476				
102	6256	6758	7281	8581	9994	11750	13906		
103	6435	6955	7498	1941	10319	12149	14402		
104	3000	<del></del>		***					
105	3000				•••				
106	3000								

TABLE B-8: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F , ELEVATION 6000 PT MSL

				STAGE VELIGET			
IND.				ATMO APTORI	,	,	
	1	2	3	•	5	6	7
1	4358	4732	5223	5842	7545	7788	
2	6652	7197	7766	9131	10964	13173	15186
,	5354	5836	6476	7288	9549	9476	•••
4	3768	4215	4666	5400	6479	7636	9630
5	5302	5729	6174	7240	8665	10376	11928
6	4193	4671	5438	6551	8094	9433	•••
7_	3963	4429	\$176	6263	7767	8547	•••
	2721	3109	3523	4193	4671	•••	***
•	4553	5190	5772	6813	8304	9952	11187
10	2799	3128	3656	4424	5446	6037	***
11	3811	4305	4832	5682	6290	•••	
73	4564	5678	5902	7100	8756	10210	•••
13	5627	6157	6997	8202	9846	10906	12495
14	4718	5175	5904	6956	8491	9336	10671
15	•	•	0		•••	•••	
16	4553	5190	5772	6813	8304	9952	11187
17	5627	6157	6997	8202	9846	10906	12405
18	10014	10014	12293	12293	14074	14074	
19	6158	6763	7616	8997	10501	12129	
20	4687	5083	5496	6404	7684	9124	10017
21	7132	7748	8346	9706	11634	13861	16285
22	7182	7650	8383	9152	10801	12602	
23	6614	7023	7661	8330	9659	11096	12698
24	5968	6863	7621	8841			
25	6885	7634	8423	9376			***
26	\$030	2276	10165	11906	13930	•••	
27	9155	10665	12295	13896			•••
28	6885	7634	9423	9376			
29	4030	8898	10165	11906	13930		
30	7749	9011	10254	11334			
31	5157	5917	6594	8011	9803		
32	4775	5178	5613	6409	7489	8749	9504
33	3999	4335	4697	\$373	6297	7364	7861
34	3962	4497	3086	5714	6894	8140	
35	4586	5203	5862	7179			
36	4472	5167	5798	7064			
37	6455	7381	8577	7004		•••	
	<del> </del>						
38	4569	5736 5373	6613				
	<del> </del>						
40	5504	6689	7918				
41	3202	3977	4724				
42	4717	5071	5964	7077			
43	5504	6689	7918				
	3202	3977	4724				
45	4712	5071	5964	7077			
46	5530	6336	7325				
47	4864	5432	6032	6665		•	•••
48	5464	6599	7846				
49	5198	5859	6665	8442		•••	
50	5845	6643	7493	9480			
51	3717	3996	4340	5015	5917		•••
52	3651	3933	4276	4900	5802	6786	
53	3775	•••				•••	
54	3638	•••					
55	5616					•••	

TABLE 8-8: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 40°F , ELEVATION 6000 PT MSL (CONTINUED)

ſ <del></del>	STAGE WEIGHT										
2304 6					<u>,                                    </u>						
	1	2	3	•	5	6	7				
56	4136										
57	4047						•				
50	4766										
59	5697					•••	•••				
60	3834	•••	• • •								
61	6736	••-					•••				
62	5569										
63	3576	4505	6080			•••					
64	2404						•••				
65	1606					•••	•••				
66	5117	6524	7800				•••				
67	3498					•••	•••				
68	3394										
69	1643						•••				
70	4238	5571	7154				•••				
71	3615	2461	•			•••					
72	2376	3092				•••	•••				
73	2761					•••					
74	838										
75	979					•••					
76	2101										
77	927					•••					
78	15893					•••					
79	5759	8981									
80	7156	9796			<del></del>						
81	5974	6926									
82	6789	10144									
83	5285	5879	6379	7444	6899	10999	12777				
14	5766	6240	6712	7885	9460	11342	13080				
85	5135	5969	6638	8090			•••				
16	4667	5389	6052	7374							
<b>0</b> 7	4030	4369	4736	5425	6364	7453	7980				
0.0	0	•									
89	4360	5349	₹305								
90	4662	5695	6840	<del></del>							
91	15711										
92	12946			<del></del>							
93	4631	5133	5868	6877	8052						
94	4446	4930	5440	6055		***					
95	4092				· · · · · · · · · · · · · · · · · · ·						
96	6126										
97	\$607	6673	7948	9221	<del></del>	•••					
98	5817										
	3245					•••					
	~~~~~	5004	5522	6146							
100	4613		1 2344		<del> </del>	<del></del>					
100	4513		50:1								
100	5460	6050	6913	3303	9476	***	334.7				
100 101 102	5460 5327	6050 5754	6198	7301	8499	>>+1	11815				
100 101 102 103	\$460 \$327 \$395	6050 5754 5830	6198 6283	7301	8499	9908 10160	11815 12035				
100 101 102 103 104	\$460 \$327 \$395 3000	5050 5754 5630	6198	7301	8499	10160	11815 12035				
100 101 102 103 104 105	\$460 \$327 \$395 3000 3000	\$050 \$754 \$830 	6198 6283 	7301 7410	8499 8636 	9988 10160	11815 12035 				
100 101 102 103 104	\$460 \$327 \$395 3000	5050 5754 5630	6198	7301	8499	10160	11815 12035				

TABLE 8-9: RUNWAY REQUIREMENTS/OFERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 80°F, ELEVATION 6000 FT MSL

	STAGE WEIGHT							
2304 #	1	2	3	1	5	6	7	
1	4358	4732	5223	5842	7545	7768		
	7902	8549	9224	10046	13023	15647	10030	
	6359	6935	7692	8657	11342	11730		
	4476	5006	5542	6415	7696	9070	11416	
	<del> </del>	<del> </del>	<del> </del>	8600	10293			
5	6297	6805	7334	<del></del>	<del> </del>	12325	14168	
	4193	4671	5438	6551	8098	9433		
7	3963	4429	5176	6363	7767	8547		
	2721	3109	3523	4193	4671			
	5408	6165	6856	6093	9864	11622	13288	
10	2799	3128	3656	4424	3486	6037		
11	4526	5114	5739	6749	7471	•••		
	5421	6032	7011	8433	10401	12127		
13	6684	7313	#311	9742	11695	12954	14735	
14	5604	6147	7013	8262	3979	11092	12676	
15	0	0	•		•••			
16	5408	6165	6056	8093	9864	11822	13288	
17	6684	7313	#311	9742	11695	12954	14735	
18	11895	11895	14601	14601	0	۰		
19	7315	8033	9047	10687	12474	14408		
20	5567	6038	6529	7607	9127	70838	12849	
21	8472	9203	9913	11529	13819	16393	19344	
22	8531	9087	9957	10871	12830	14969	•••	
23	7856	8342	9100	9894	11473	13179	15083	
24	5968	6863	7821	8841		***		
25	8178	9068	10005	11137			•••	
26	9539	10569	12074	14142	16567			
27	10875	12668	14604	16506		•••		
28	8178	9068	10005	11137		•••	•••	
29	9539	10569	12074	14142	16547	•••		
30	9204	10703	12180	13463		•••		
31	6125	7029	7832	9516	11644			
32	5672	6252	6667	7613	8895	10392	11289	
33	4750	5149	5579	6382	7480	8747	9161	
34	4730	5342	6042	6787	8188	9669		
35	5447	6280	6963	8528				
36	5227	6151	6907	8415				
37	7667	8767	10188					
38	5562	6813						
39	5427	6382	7855					
40	6538	7945	9405					
41	3804	4724	5622	•				
42	5596	6024	7084	8406				
43	6538	7945	9405					
44	3804	4724	5611	<del> </del>				
45	5596	6024	7084	8406				
46	6569	7526	8701				***	
47	5778	6452	7165	7917				
48	6490	7838	9320					
	<del> </del>	<del></del>	<del></del>	<del> </del>				
49	6174	6959	7917	10027	<del> </del>		· · · · · · · · · · · · · · · · · · ·	
50	6943	7890	6901	11261			•	
51	4415	4749	5156	5957	7028			
52	4339	4674	5082	5823	6895	8065		
53	4484						***	
54	4559							
55	6670					***		

TABLE B-9: RUNMAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR, TEMPERATURE 80°F, ELEVATION 6000 FT MSL (CONTINUED)

		· · · · · · · · · · · · · · · · · · ·		STAGE WEIGHT			
Z706 #	1	2	3	•	s	6	7
56	4136						
57	4807						
58	\$661						
59	6766				•		
60	4555						
61	8001						
63	6615						
63	6616	5561	7505				
64	2855					•••	•••
65	1902						
66	6317	8054	9629				
67	4328						
68	4189					•••	
69	2028				***		
70	\$207	6876	6631				
71	2487	3018	0				
72	2933	3817	•••				
73	3408		•••				
74	1034				***		
75	1208		**-		•••	•••	
76	2593		***				
77	1145		•••		•••		
78	18878		•••		•	•••	•••
79	6840	10668	•				•••
80	8580	11636					
81	7374	11018					
82	8381	0					
83	6277	6983	7577	8842	10570	13065	15177
84	6848	7412	7973	93\$6	11237	13473	15537
85	6100	7090	7884	9609	•••		•••
86	5544	6401	7188	8759			•••
87	4787	5190	5626	6444	7559	8853	9478
66	0	•	•		•••		
89	5178	6354	7489	•••			•
90	5538	6764	8124				•••
91	18717						
92	15377	•••					
93	5501	6097	6970	\$169	9565	•••	
94	5281	5856	6462	7193	•••	•••	
95	4860						
96	7277	•••	•				
97	6660	7926	9440	10953			
98	6909						
"	3855						
100	4513	5004	5522	6146			
101	5460	6050	6913	8092	9476		
102	7503	\$107	6737	10302	12006	14124	16729
103	7878	8519	9187	10851	12665	14926	17713
104	3000						
105	3000						
106	3000	•••					
107	3000	•••			•••		

#### APPENDIX C

#### AIRPLANE RUNUP OPERATIONS

This Appendix discusses the adaptation of an existing INM equation for use in computing runup noise within INM Version 4.11. This equation, also used in the Time-Above-Threshold (TA) equation, can be used to approximate the maximum A-weighted sound level  $(L_{\text{MMX}})$  and the maximum tone-corrected perceived noise level  $(\text{PNLT}_{\text{MAX}})$  for a one-second time period as follows:

$$L_{\text{AMAX}} = \text{SEL} - 10\log_{10}[((500\pi)/(V))(.001R_0)^{(k)}] \text{ and}$$
 (1)

$$PNLT_{MAX} = EPNL - 10log_{10}[((500\pi)/(V))(.001R_0)^{(k)}] + 10,$$
 (2)

> EPNL = the Effective Perceived Noise Level from the Noise-Power-Distance data base (dB);

V = the airplane velocity (ft/sec);

R<sub>0</sub> = the closest point of approach
from airplane to receiver (ft);

k = a constant exponent with a fixed
value of 0.6 in the INM; and for
Equation (2),

10 = a duration correction as discussed in Section 2.3, Equation (2).

The above equations assume: (1) an approximate shape of an airplane's sound level time history; and (2) symmetry in the time history trace around the  $L_{\text{AMAX}}$  or PNLT<sub>MAX</sub>, as appropriate. The  $L_{\text{AMAX}}/\text{PNLT}_{\text{MAX}}$  values computed with these equations were verified using measured  $L_{\text{AMAX}}/\text{PNLT}_{\text{MAX}}$  data in the literature. 1

Given the computed  $L_{\text{MMAX}}/\text{PNLT}_{\text{MAX}}$  and the user-defined duration and location for a runup, the SEL/EPNL for the runup is computed by multiplying the acoustic energy associated with the  $L_{\text{MMAX}}/\text{PNLT}_{\text{MAX}}$  by the user-defined duration, and converting the total runup energy to a decibel value as follows:

$$SEL_{MAX} = 10\log_{10}[(DUR)10exp(L_{MAX}/10)] \text{ and}$$
 (3)

where	$\mathtt{SEL}_{\mathtt{RUNUP}}$	=	the Sound Exposure Level for the runup (dBA);
	EPNLRUNUP	=	the Effective Perceived Noise Level for the runup (dB);
	DUR	=	the user-defined duration of the runup (seconds);
	L <sub>AMAX</sub>	=	the maximum A-weighted sound level computed, using Equation (1);
and	PNLT <sub>MAX</sub>	=	the maximum tone-corrected perceived noise level computed, using Equation (2).

The  $SEL_{RUNUP}$  value from Equation (3) is then used to complete the noise exposure due to runup operations for all INM noise metrics, except NEF and WECPNL. The noise exposure due to runup operations for NEF and WECPNL are computed using the EPNL\_RUNUP value from Equation (4).

#### C.1 Verification

The runup enhancement within INM Version 4.11 was verified using measured runup noise level data for the A320 airplane with the newer CFM56-5-A1 engine, and the B747 airplane with the older JT9D-7A engine.<sup>2,3</sup> The measured data for the A320 agree extremely well with INM-predicted data, i.e., ± 3 dB with a mean difference of .6 dB and a standard deviation of 2.2 dB, for receivers located at angles of 0, 45, 90, 120, 135, and 180 degrees relative to the nose of the airplane. Note: At 180 degrees, the data used for comparison with the predicted levels were obtained by linear extrapolation of measured data. The agreement between measured and predicted data at the above six receiver locations was essentially independent of thrust for thrusts of 78, 86, and 90 percent N1. At the 150 degree location, the agreement was only modest. INM Version 4.11 overstated the noise by approximately 6 dB at thrust levels of 86 and 90 percent N1, and by almost 12 dB at 78 percent N1. Similar results were observed for the B747 airplane at all receiver locations.

The agreement between measured and predicted runup noise levels could be improved if the INM maintained a detailed data base of measured runup directivity patterns for all airplanes as a function of distance and thrust. In lieu of developing such a substantial and potentially costly data base, the simplified

directivity pattern discussed in Appendix A is a reasonable approximation of runup directivity.

#### C.2 References

- Bishop, D.E., Beckman, J.M., Bucka, M.P., <u>Revision of Civil Aircraft Noise Data for the Integrated Noise Model (INM)</u>, Report No. 6039, Project No. 04453, Canoga Park, CA: BBN Laboratories Incorporated, September 1986.
- 2 <u>A320 Noise Definition Manual NDM</u>, FRANCE: Airbus Industrie, 1990.
- An Excerpt from the Model B747 Flight Manual, <u>A-Weighted Noise Level Contours</u>, Seattle, WA: Boeing Commercial Airplane Company, 1986.

#### APPENDIX D

#### INM INPUT TESTCASE

This Appendix presents a copy of the INM Input Testcase, revised to reflect several INM Version 4.11 enhancements. The revised Testcase includes an airplane runup definition, and an approach runway threshold definition. The entry related to data base selection, contained in the PROCESS section of previous versions of the Input Testcase, has been deleted; the ACDB11.EXE computer program, included with the INM Version 4.11 release, should be used to access/print all elements of Data Base Number 11. The Input Testcase contained herein is included with the Version 4.11 release.

#### BEGIN.

#### SETUP:

TITLE CAMBUAL AVERAGE EXPOSURE AT AN EXAMPLE OF A MEDIUM HUB AIRPORT-AIRPORT CEXAMPLE MHA>

ALTITUDE 0 TEMPERATURE 59 F

RUMMAYS

RM 09L-27R 0 0 TO 9487 -497 HEADING-93 RW 27L-09R 4203 -1410 TO -6920 -1044 HEADING-272 RW 35-17 7355 1366 DT 100 TO 6407 6742

#### AIRCRAPT:

AC 747200 AC 747200 AC DC1030 AC DC870 AC A300 AC 757PM AC 727015 AC DC930 AC MD81 AC 737300 AC SABREO

AC BECSEP
AC S-76 CURVE-250C30 PARAM-HELI STAGE 1-HORFLT
CATEGORY-PGA

MOISE CURVES

#### 3 BY 8 3 BY 6 NC 250C30 RPML. THRUSTS 91.2 87.2 84.5 80.7 75.1 97.2 200 90.2 85.8 83.1 93.1 400 90.6 87.4 82.6 600 79.4 73.7 67.6 1000 2000 77.2 73.7 4000 68.2 63.8 6000 63.1 10000 57.4 68.7 56.8 SEL THRUSTS 2 3 88.6 84.2 90.0 85.6 95.6 200 400 600 81.5 77.8 82.9 79.1 89.0 85.8 1000 2000 72.1 73.5 81.0 66.0 66.6 75.6 72.1 4000 6000

#### APPROACH PARAMETERS

AP HELI WEIGHT=10000 ENGINE=2 STOP=1 PINSP=160 TAXI=160 LNDFPS=3

INT.NM.

#### PROFILES APPROACH

PF ALT3D SEGMENTS=7
DISTANCES 20. 10. 5. 3. 1. -.164 STOP
ALTITUDES 6000 3236 1644 1007 370 0 0
SPEEDS TERMSP INTSP APPSP FINSP LNDSP REVSP TAXI
THRUSTS INTFIS APPFAS LNDFFS LNDFLS REV IDLE

PF COPTR SEGMENTS=7
DISTANCES 3.9 3.1 2.4 1.6 0.8 0 0
ALTITUDES 2500 2000 1500 1000 500 0 0
SPEEDS FINSP FINSP FINSP FINSP FINSP FINSP FINSP TAXI
THRUSTS LNDFFS LNDFFS LNDFFS LNDFFS LNDFFS

ECHO.

FT.

#### PROPILES TAKEOFF

PF	HORFLT	SEGMENTS=8	WEIGH	r=10000	ENGINE.	S=2			
	DISTANCE	S 0	1376	4126	6876	6877	9626	10000	15000
	ALTITUDE	S 0	0	500	1000	1000	1500	1500	1500
	SPEEDS	32	160	160	160	160	160	160	160
	THRUSTS	2	2	2	2	1	1	1	

#### COMMENTS:

Note: Standard conditions have been defined. To implement the takeoff profile generator see Section 2.1. In addition, the elevation enhancement has not been selected. To implement elevation see Section 2.2.

Note: A runway touch-down point of 1054 ft has been defined for approach operations on Runway 35 (i.e., 100 ft for the user-defined D7 plus 954 ft for the fixed touch-down point).

#### THY . IM.

```
TARBOFFS BY FREQUENCY:
   OPER DC930 STAGE 1 D-26.5 N-.5 STAGE 2 D-6 N-.5
      STAGE 3 D=1.5
OPER HD81 STAGE 2 D=1.0
OPER 737300 STAGE 1 D=1.5 N=.5
   TRACK TR2 RWY 27R STRAIGHT 4.1 LEFT 86 D 1.6 STRAIGHT 50
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=3 STAGE 3 D=1
STAGE 4 D=1 STAGE 5 D=.5 STAGE 6 D=.5
OPER DC670 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1
                             STAGE 3 D=1 STAGE 4 D=2.5 STAGE 5 D=1
      STAGE 6 D=.5

OPER A300 STAGE 2 D=2 STAGE 3 D=1

OPER 727Q15 STAGE 1 D=6 N=1 STAGE 2 D=4.4 N=1.4 STAGE 3 D=1.8
   TRACK TR3 RWY 09R STRAIGHT 1.3 LBFT 15 D 1.0 STRAIGHT 1.4
                                   RIGHT 57 D 1.8 STRAIGHT .5 RIGHT 50 D 1.6 STRAIGHT 50
      OPER DC870 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1 STAGE 3 D=1 STAGE 4 D=1.5 STAGE 5 D=.5

OPER 757PW STAGE 3 D=2.5

OPER 727Q15 STAGE 1 D=21 N=2.5 STAGE 2 D=16.5 N=4 STAGE 3 D=8 N=.5

OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5 STAGE 3 D=1.5

OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5 STAGE 3 D=1.5
      OPER MD81 STAGE 1 D= 3 N=.5
OPER 737300 STAGE 2 D=.5
  TRACK TR4 RWY 27R STRAIGHT 4.1 LEFT 230 H 2.2 STRAIGHT 50 OPER SABR80 STAGE 1 D=3 N=.1
  TRACK TRS RWY 35 STRAIGHT 50
OPER SABRSO STAGE 1 D=30.5 N=2.5
OPER BECSSP STAGE 1 D=13 N=1
  TRACK TR6 RWY 17 STRAIGHT 50
      OPER SABREO STAGE 1 D=12.5 N=.5
OPER BECSEP STAGE 1 D=30 N=3
```

TRACK TR7 RWY 17 STRAIGHT 1.5 RIGHT 265 H .25 STRAIGHT 3
LEFT 245 H 1.0 STRAIGHT 50
OPER S-76 STAGE 1 D=5 LANDINGS BY PERCENTAGE:

OPER 747200 PROF-STD3D D-3 N-0 OPER DC1030 PROF-STD3D D-22 N-2 OPER DC870 PROF-ALT3D D-22 N-2 OPER A300 PROF-STD3D D-2 N-1 OPER 757PW PROF-STD3D D-6 N-1 OPER 727Q15 PROF-ALT3D D-70 N-10 OPER DC930 PROF=ALT3D D=70 N=4 OPER MD81 PROF=STD3D D=4 N=.5 OPER 737300 PROF-STD3D D=1.5 N=.5 OPER SABREO PROF-STD3D D=25 N=2 OPER BEC58P PROF-STD5D D=42 N=5 PROF-COPTR D-5

TRACE TRE RWY 27R STRAIGHT 50 RIGHT 82 D 1.5 STRAIGHT 4.2 PERCENT COM-72 GA-0

TRACK TR9 RWY 09R HEADING 260 STRAIGHT 50 RIGHT 272 H 1.5 STRAIGHT 7 PERCENT COM-28 GA-0

TRACK TRIO RWY 35 STRAIGHT 50 PERCENT COM-0 GA-30

TRACK TR11 RWY 17 STRAIGHT 50 PERCENT COM=0 GA=70

TOUCHNGOS BY FRROUENCY:

TRACK TR14 RWY 17 STRAIGHT 3 LEPT 180 D 2.0 STRAIGHT 6 LEFT 180 D 2.0 STRAIGHT 3
OPER BEC58P STAGE 1 PROF STD5D D=23

#### COMMENTS:

Mote: A runup operation has been defined for the B747-200 airplane. The runup takes place at the start of Runway 09L and lasts for 10 seconds, (i.e., in terms of average yearly duration).

PROCESSES:

PT.

MONARM.

GRID NEF LDW TA START=-3000 1500 STEP=1000 700 SIZE=2 BY 3

GRID LEQ TA DBA=75 START=11000 3000 STEP=0 0 SIZE=1 BY 1 DETAIL

COMTOUR LDW AT 65 75
PLOT SIZE=11 8.5 SCALE=8000

MMD.

#### APPENDIX E

#### WINM USER'S MANUAL

This Appendix contains a copy of the User's Manual for the WINM computer software, an INM Version 4.11 plotting program for use with Microsoft Windows. The WINM software and its User's Manual, contained herein, were prepared by the SysTeam Corporation under contract to the FAA.

# WINM

Windows Plotting Program
Supplement to Integrated Noise Model Version 4.11

# User's Manual

November 17, 1993

Prepared by:

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SysTeam Corporation Gaithersburg, MD

Prepared for:

Federal Aviation Administration Washington, DC

FAA Contract # DTFA01-92-Y-01042 Task Order #1

#### 1.0 INTRODUCTION

This User Guide is a combined tutorial-manual that comes to you as part of WINM 4.11.

# 2.0 OPERATIONAL REQUIREMENTS

#### Software/Hardware Requirements

WINM has the same software and hardware requirements as Microsoft Windows 3.x.

# 3.0 INSTALLATION

Before you start, make sure that you have all the material supplied with WINM 4.11 and check that your equipment matches the list in Chapter 2.

#### Installation Procedure

WINM comes with four files under the directory \INM411. These files will be installed as part of the primary INM installation. They are:

WINM.EXE

- The window plot program for INM

INMINPUT.TST

- Test case version of input data

CONTOURS.TST

- Test case version of contour data

INMCOLOR DATA - Color control file

#### Windows Installation of WINM

- Start up Windows by typing WIN.
- Open Windows' Program Manager.
- Open the Windows File menu. Select New.
- The New Program Object dialog box will appear.
- Select Program Group and click on OK.
- The Program Group Properties dialog box will appear.
- Type WINM in the Description field. Click on OK.
- Open the Windows <u>File</u> menu. Select <u>New</u>.
- The New Program Object dialog box will appear.
- Select Program Item and click on OK.

• The *Program Item Properties* dialog box will appear. Enter the text in the fields as indicated:

For Window 3.1 environment:

Description: WINM v4.11

Command line: C:\INM411\WINM Working Directory: C:\INM411

Shortcut Key: None

For Windows 3.0 environment:

Description: WINM 4. 11

Command line: C:\INM411\WINM

Shortcut Key: None

- Click on OK.
- Run WINM by double clicking the WINM icon.

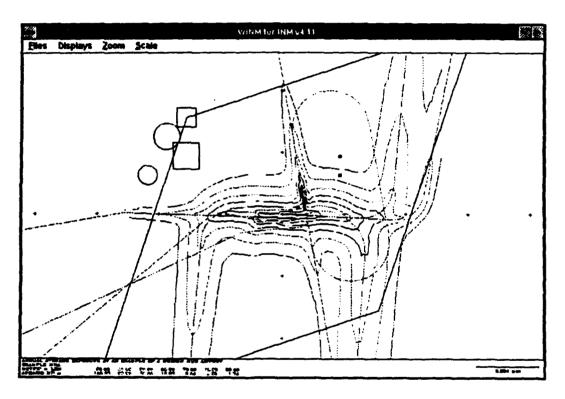
#### 4.0 TUTORIAL

#### **About the Tutorial**

The tutorial has been structured so that the exercises will give you progressive familiarity with the operations that you will carry out within WINM 4.11.

# 4.1 Loading INM Files

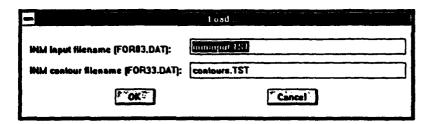
The starting point for this exercise is the default screen you see as soon as you start WINM 4.11 from the Windows *Program Manager*.



By default, WINM uses two default INM input files. To load a different set of input files,

- Place the mouse pointer arrow on Files in the menu bar; and
- Click once on the left mouse button.
- In the menu, click the mouse pointer on Load.

See the Load dialog box.



## About the Load Dialog Box

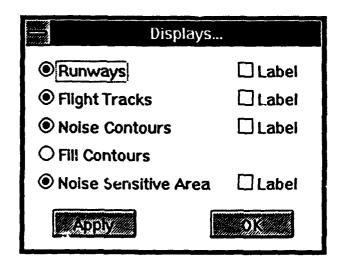
This menu option loads the INM input file and INM contour file. By default, test files "inminput.TST" "contours.TST" are chosen. Examples of standard input files are in the square brackets.

For this exercise, the default selections will not be changed. If you desire to select another set of INM input files in the future, use the *Tab* key to highlight the appropriate text field, then press the *Backspace* key to delete the default entry. Type in the appropriate file name. When correct, click on *OK*. For now, click on *Cancel* to close this window and continue with the tutorial.

# 4.2 Adjusting the Data Display Information

In the menu, click the mouse pointer on Displays.

See the Displays dialog box.



#### About the Displays Dialog Box

This menu option allows the user to select which data display information is to be shown. Select any option one at a time and click on Apply to see its effect immediately. Experiment with as many combinations as you like. Text labels may be independently selected for each displayed item type by clicking on the Label box next to each item.

# 4.2.1 Runways

This radio button turns on/off the display of the runways.

# 4.2.2 Flight Tracks

This radio button turns on/off the display of the flight tracks.

#### 4.2.3 Noise Contours

This radio button turns on/off the display of the noise contours.

#### 4.2.4 Fill Contours

This radio button turns on/off the option to fill the contours.

#### 4.2.5 Noise Sensitive Area

Although every one of these options depends on the INM input files selected, the Noise Sensitive Area is a special option. This menu option displays user-defined sensitive noise areas. These areas are defined after the END statement of the INM input data file (FOR03.DAT), and each can be either a polygon, square, circle, or point. The area can be defined in NM or FEET and a descriptive text label for label description of the area can be inserted after an asterisk (\*) at the end of the line. The user can input/modify these data before or after running the noise model (but not during running the WINM program). The following shows an example of the descriptive text labels as seen in the default INM input filename 'inminput.TST':

#### NOISE-AREA

P NM -10.0 -10.0 -5.0. 5.0 10.0 10.0 5.0 -5.0 \* Poly Area C NM -7.0 2.0 0.5 \* Circle 1 C NM -6.0 4.0 0.7 \* Circle 2 R NM -5.0 5.0 0.5 0.5 \* Rect 1 R NM -5.0 3.0 0.7 0.7 \* Rect 2 M NM 3.0 3.0 \* Point 1 M NM 3.0 2.0 \* Point 2 M FT 3000.0 1000.0 \* Point 3 M FT 5000.0 2000.0 \* Point 4

The formats for these areas are defined as follows:

#### **NOISE-AREA**

- P <NM> <X1> <Y1> <X2> <Y2> ... <Xn> <Yn> \* <Polygon Label>
  Polygon area defined in NM followed by a series of X, Y points in NM with a label of Polygon Label'.
- C <FT> <Xc> <Yc> <Radius> \* <Circle Label>
  Circle area defined in FT with its center at Xc, Yc, and its Radius with a label of 'Circle Label'.
- R <FT> <Xc> <Yc> <Width> <Height> \* <Rectangular Label>
  Rectangle area defined in FT with its center at Xc, Yc, and its Width and
  Height from the center with a label of 'Rectangular Label'.
- M <NM> <X> <Y> \* <Point Label>
  Mark point defined in NM at X, Y with a label of 'Point Label'.

Click on OK to leave the Displays dialog box.

## 4.3 Zoom

#### About the Zoom Menu

WINM 4.11 offers you the capabilities to zoom in/out of various sections of the display for specialize viewing.

We will now become familiarized with the zooming capabilities within WINM 4.11.

- Place the mouse pointer arrow on **Zoom** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down Zoom menu appear.

• In the menu, click the mouse pointer on **Zoom In**.

A zoom box will appear in the center of the screen.

- Move the mouse to expand/shrink the zoom box.
- If you desire to move the zoom area, hold down the right button and drag the zoom box to a different area.
- Click the left button to accept zoom.

Note! At any time, click the right button to cancel the zoom box.

Zoom Qut works similar to Zoom In.

- Place the mouse pointer arrow on **Zoom** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down **Zoom** menu appear.

• In the menu, click the mouse pointer on Zoom Qut.

A zoom box will appear.

- Move the mouse to expand/shrink the zoom box.
- If you desire to move the zoom area, hold down the right button and drag the zoom box to a different area.

Click the left button to accept zoom.

Note! At any time, click the right button to cancel the zoom box.

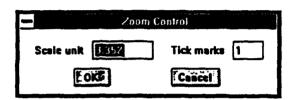
Zoom Control allows you more precise zoom control.

- Place the mouse pointer arrow on the Zoom menu; and
- Click once on the left mouse button.

You will see the drop-down Zoom menu appear.

• In the menu, click the mouse pointer on **Zoom Control**.

See the Zoom Control dialog box.



This menu option allows you to set the scale value to a specific scale (i.e. 3.352 nm per scale unit) and to set the number of tic marks between the scale unit marks (default is 1). You can change these values anytime.

For now, let's continue with the exercise. Click on Cancel to leave the Zoom Control dialog box.

#### 4.4 Scale

#### About the Scale Menu

WINM 4.11 offers you the capabilities to change the scale on which the display units.

We will now become familiarized with the scaling capabilities within WINM 4.11.

- Place the mouse pointer arrow on Scale in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down Scale menu appear.

• In the menu, click the mouse pointer on any of the menu selections to see its effect to the scale shown at the bottom right-hand corner.

We have now covered the major capabilities of WINM 4.11.

Let's print the display to a printer.

- Place the mouse pointer arrow on Files in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down Files menu appear.

• In the menu, click the mouse pointer on *Print*. A submenu will appear.

#### 4.5 Print

# **About the Print Menu Option**

This menu option allows a hard copy output to a printer. The printout will go to the default printer which can be set via Printers in Control Panel.

#### Actual Scale

This menu option allows the user to print the current screen for scaling. The scale unit will reflect 1 inch on the hardcopy printout.

#### Screen Zoom

This menu option allows the user to print the current screen at the current zoom factor. The left and right edges of the hardcopy printout will be set to match the left and right edges of the screen display. If the printer's page orientation is set to 'Landscape' in the Windows *Print Manager*, then the top and bottom edges of the hardcopy printout will be set to match the top and bottom edges of the screen display as well.

To print what is displayed, select Screen Zoom.

You can now exit the program.

- Place the mouse pointer arrow on Files in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down Files menu appear.

• In the menu, click the mouse pointer on Exit.

This menu option exits the program. The current display setup (contours on/off, tracks on/off, etc.) will be saved when the program is restarted, this setup will be recalled.

CONGRATULATIONS!! You have completed the tutorial.

# 5.0 Others

#### **Move Origin**

The user can move the origin by clicking on a point using the mouse's right button, holding it down, and dragging it to a new location.

#### Colors for Display

The user can modify the colors displayed on screen by modifying the appropriate fields in the file INMCOLOR.DAT. For every increment of 16 colors (up to 256), a new fill pattern will be automatically introduced. The user can modify the color file until the desired colors/patterns are found. Note that the ordering of these colors as they appear in the file is very crucial. An example is as follows:

```
/* Runway Clr */
4
2
      /* Landing_Track_Clr */
3
      /* Takeoff_Track_Clr */
      /* Touchngo Track_Clr */
6
255
      /* Level 40 Less_Clr */
237
      /* Level 41 To 45 Clr */
173
      /* Level_46_To_50_Clr */
27
      /* Level 51 To_55 Clr */
102
      /* Level_56_To_60_Clr */
85
      /* Level 61 To_65_Clr */
68
      /* Level_66_To_70_Clr */
50
      /* Level_71_To_75_Clr */
      /* Level 76 To 80 Clr */
140
      /* Level 81 Greater Clr */
17
```

# Help

Help is not available directly from the program. For technical problems, please contact your distributor.

# 6.0 Program Limitation.

- Maximum 2000 points per noise contour.
- Runways information input is in FEET (from INM input file).
- Tracks information input is in NM (from INM input file).
- Shade pattern on hard copy may not be the same as on the screen due to the incompatibility number of colors support by the display and the printer.